

Millimeter Wave Receivers for QUIJOTE CMB polarization experiment

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EPI 2013 Conference

**Santander
27th June 2013**



- **Q-U-I JOint TEnerife** (Stokes parameters Q, U and I)
- **Cosmic Microwave Background (CMB) polarization receivers**
- **To obtain polarization maps in the frequency range 11- 40 GHz**
- **Angular resolution: ~1 degree**



Instituto de Astrofísica de Canarias (IAC), Tenerife (Spain): Coordinator



Instituto de Física de Cantabria (IFCA), Santander (Spain)



Universidad de Cantabria (UC), Santander (Spain)



University of Cambridge, (UK)



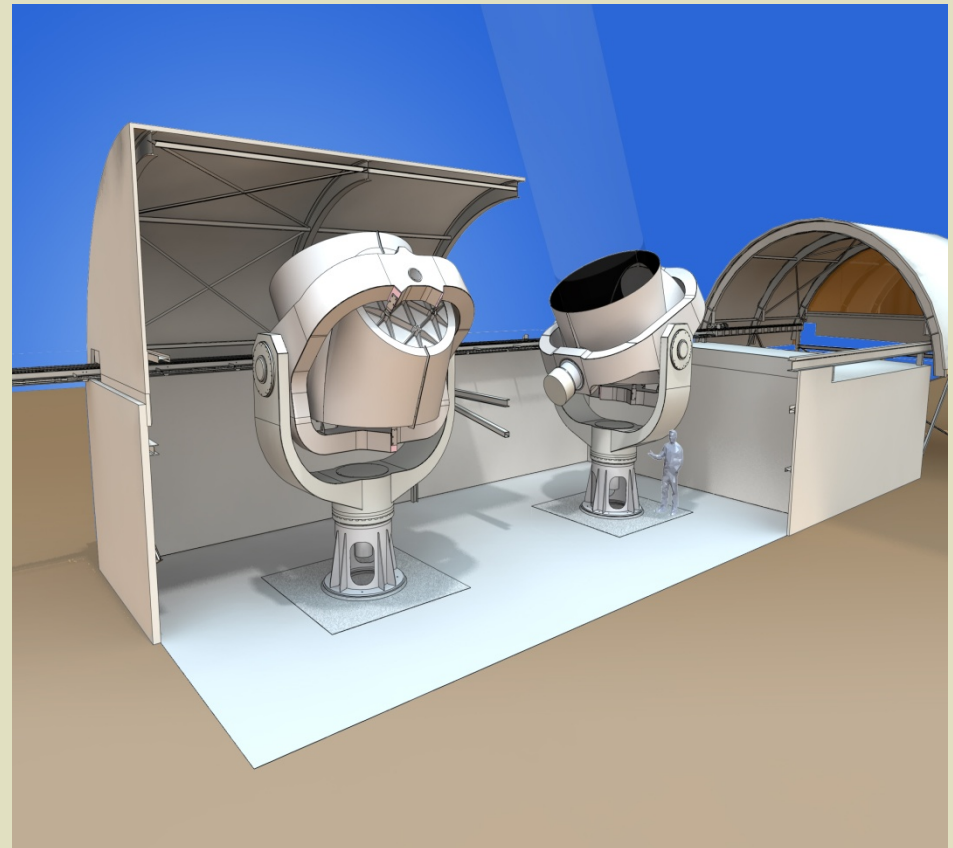
University of Manchester, Jodrell Bank Centre for Astrophysics (UK)



IDOM, Bilbao (Spain)



Izaña site, 2.390 m



**QUIJOTE Instruments 1 and 2
and enclosure**

- Polarimeters: polarisation Stokes parameters (Q, U and I) Cosmic Microwave Background (CMB) and other processes of Galactic and extragalactic emission.
- Angular resolution of ~ 1 degree

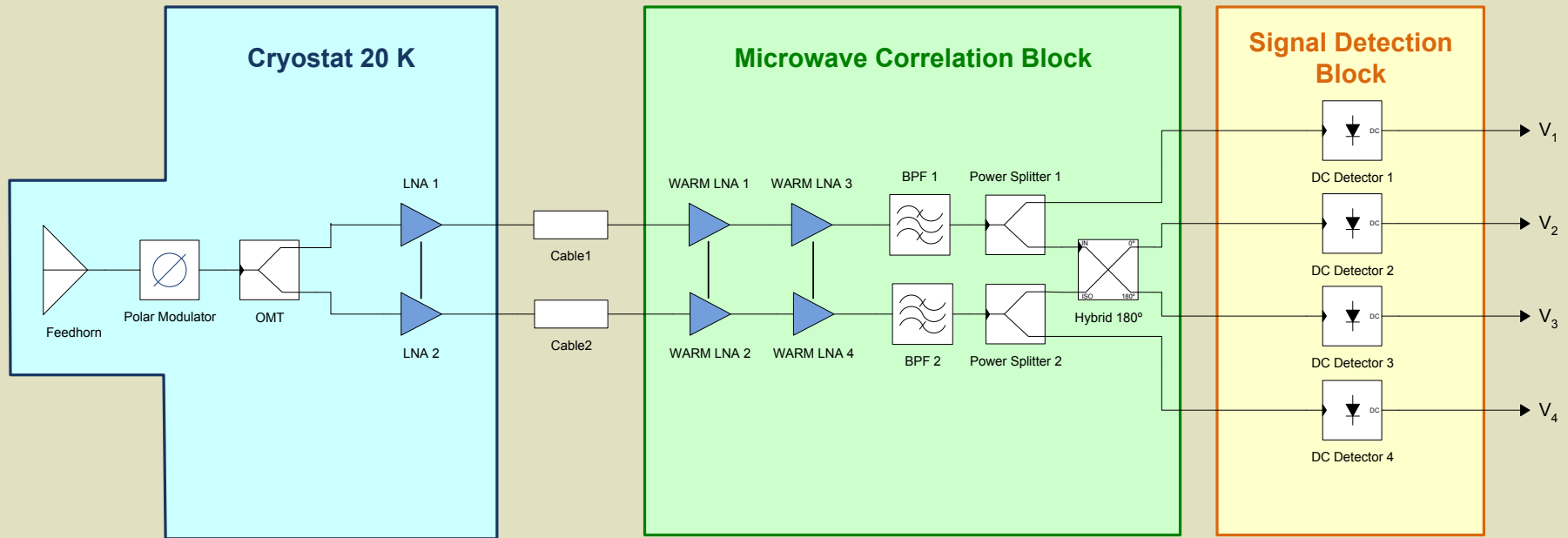
QUIJOTE-CMB Experiment. Nominal characteristics of the three instruments: MFI, TGI and FGI.

	MFI				TGI	FGI
Nominal Frequency [GHz]	11.0	13.0	17.0	19.0	30.0	40
Bandwidth [GHz]	2	2	2	2	8	10
Number of horns	2	2	2	2	31	40
Channels per horn	4	4	4	4	4	4
Beam FWHM [°]	0.92	0.92	0.60	0.60	0.37	0.28
T_{sys} [K]	25.0	25.0	25.0	25.0	35.0	45.0
NEP [$\mu\text{K s}^{1/2}$]	280.0	280.0	280.0	280.0	45.0	50.0
Sensitivity [$\text{Jy s}^{1/2}$]	0.30	0.42	0.31	0.38	0.06	0.06

MFI = Multi-Frequency Instrument (First Instrument: QUIJOTE 1)

TGI = Thirty-GHz Instrument (Second Instrument: QUIJOTE 2)

FGI = Forty-GHz Instrument



Simultaneous Q and U detection

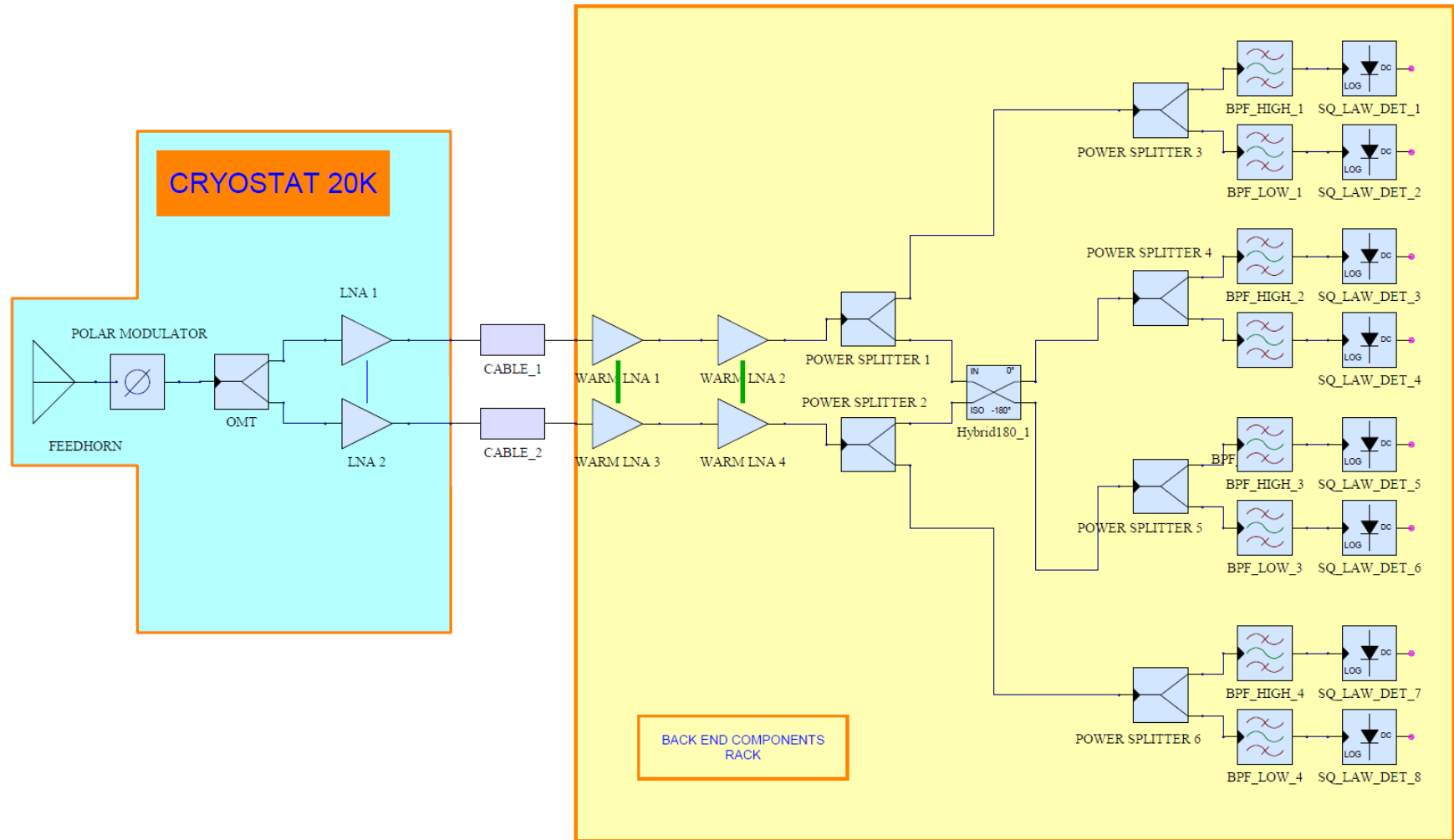
$$V_j = \frac{1}{2} I_j + \frac{1}{2} Q_j \cos(4\varphi + \theta_j) + \frac{1}{2} U_j \sin(4\varphi + \theta_j)$$

$$\theta_1 = 0; \quad \theta_2 = \pi; \quad \theta_3 = +\frac{\pi}{2}; \quad \theta_4 = -\frac{\pi}{2}$$

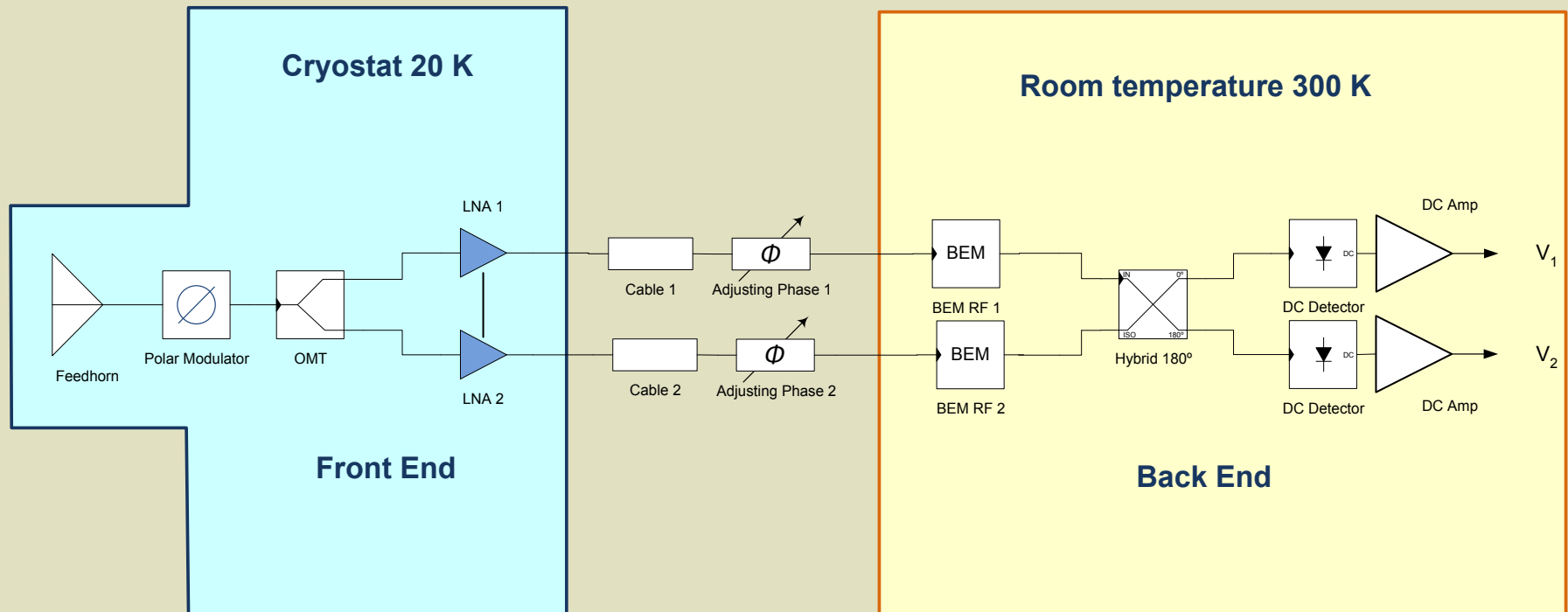
Q , U and I = Stokes parameters

φ = Position angle of the modulator

These parameters depend on the time
and on the channel ($j = 1, 2, 3, 4$)



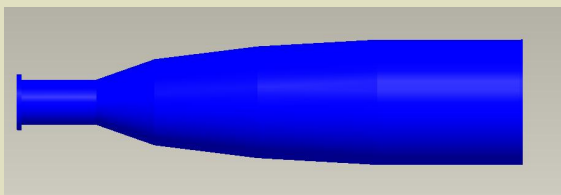
Low frequency channels: 11-13 GHz and 17-19 GHz: eight channels per pixel



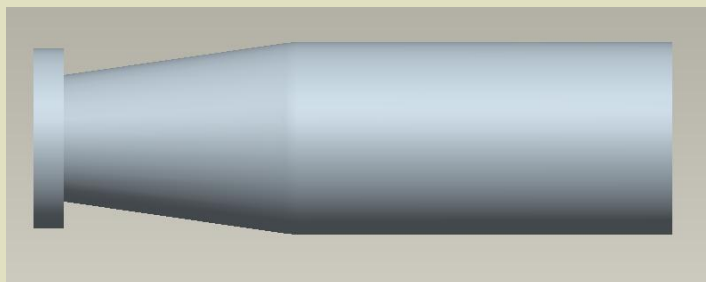
Modulator to stabilize gain drift. Simple design: two channels per pixel.



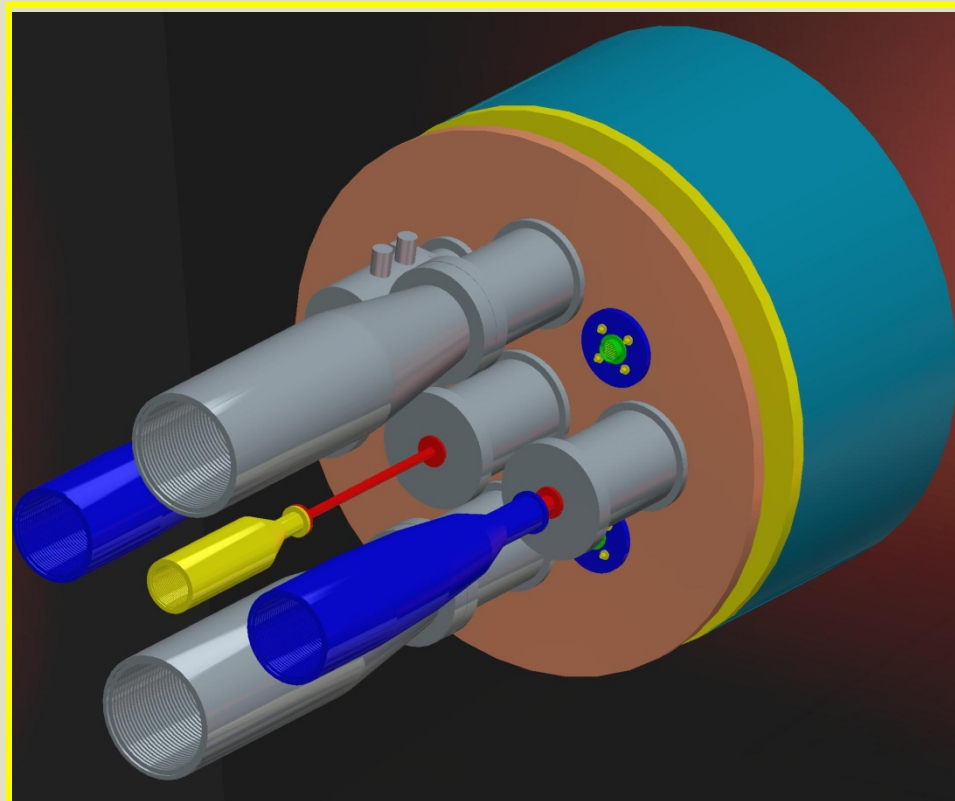
26-36GHz Horn

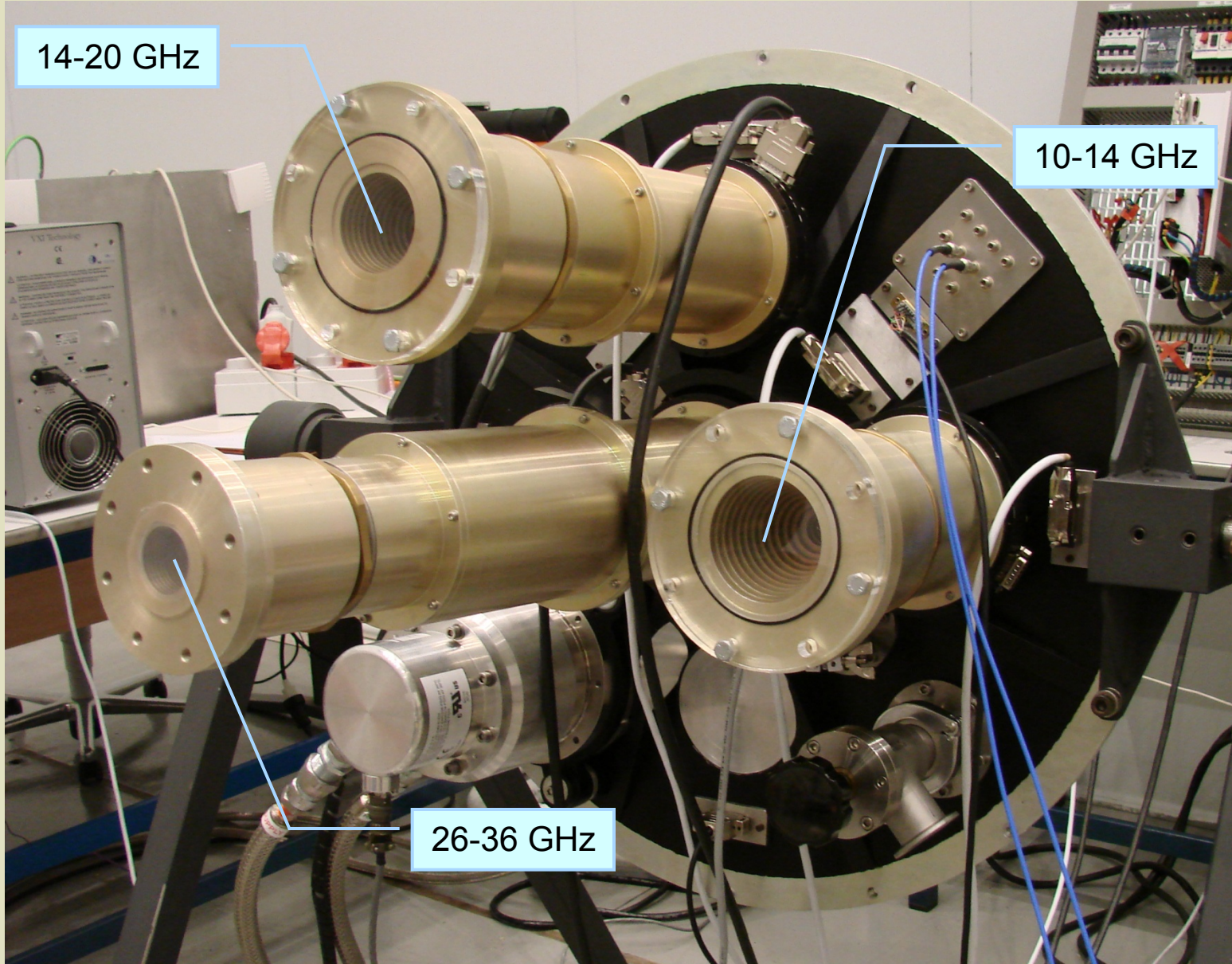


14-20GHz Horn



10-14GHz Horn



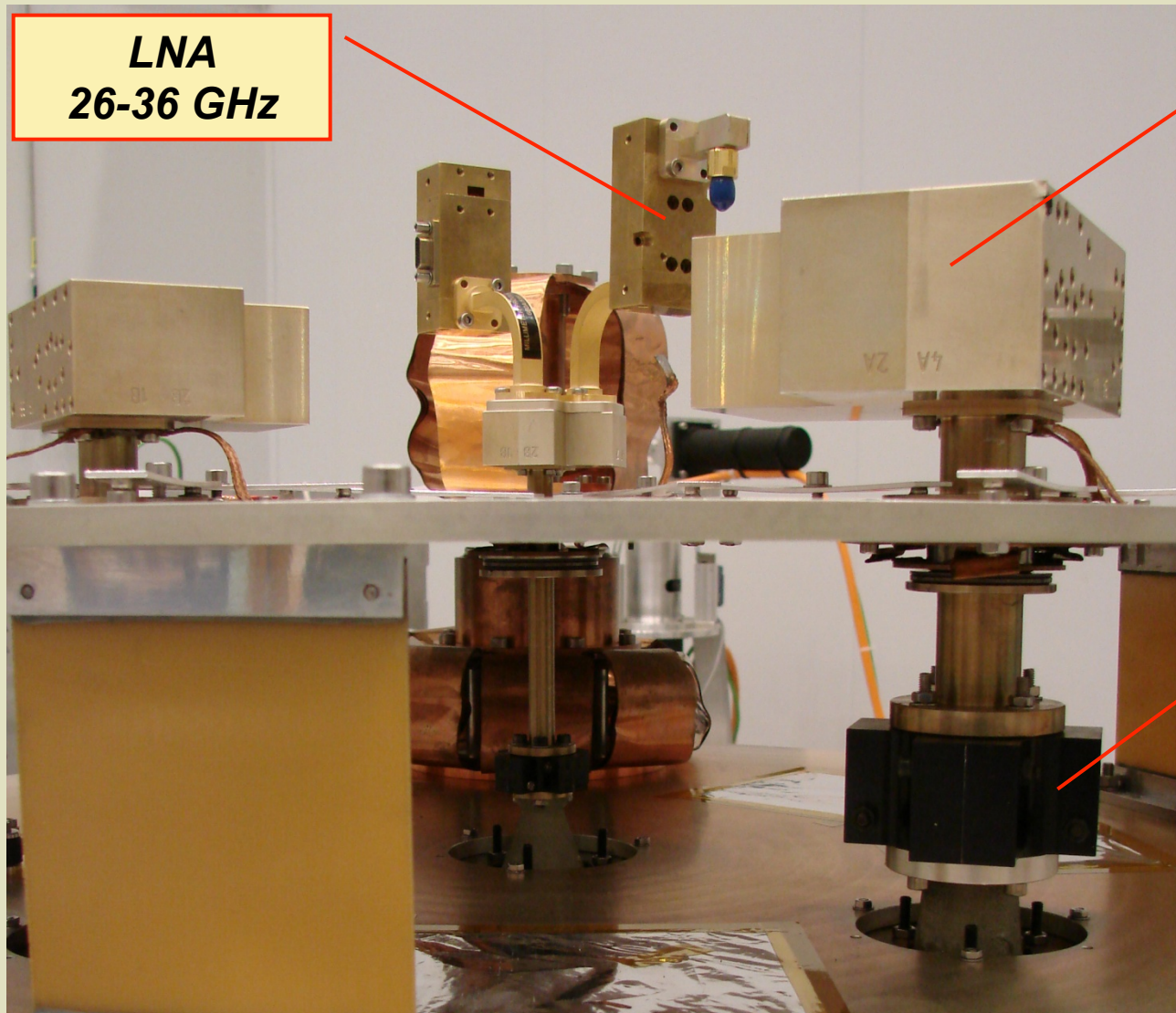


14-20 GHz

10-14 GHz

26-36 GHz

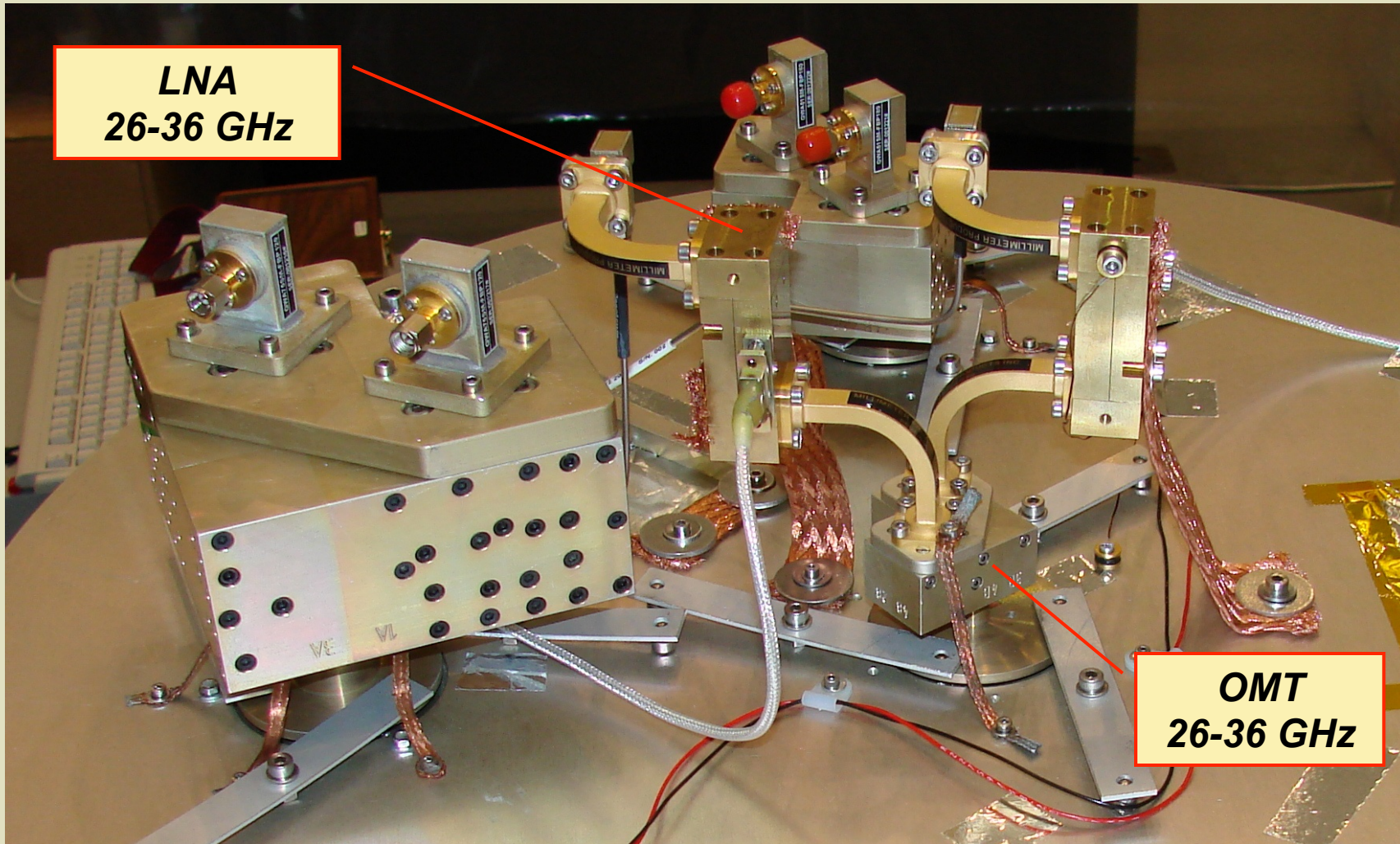
QUIJOTE MFI: Receivers integration

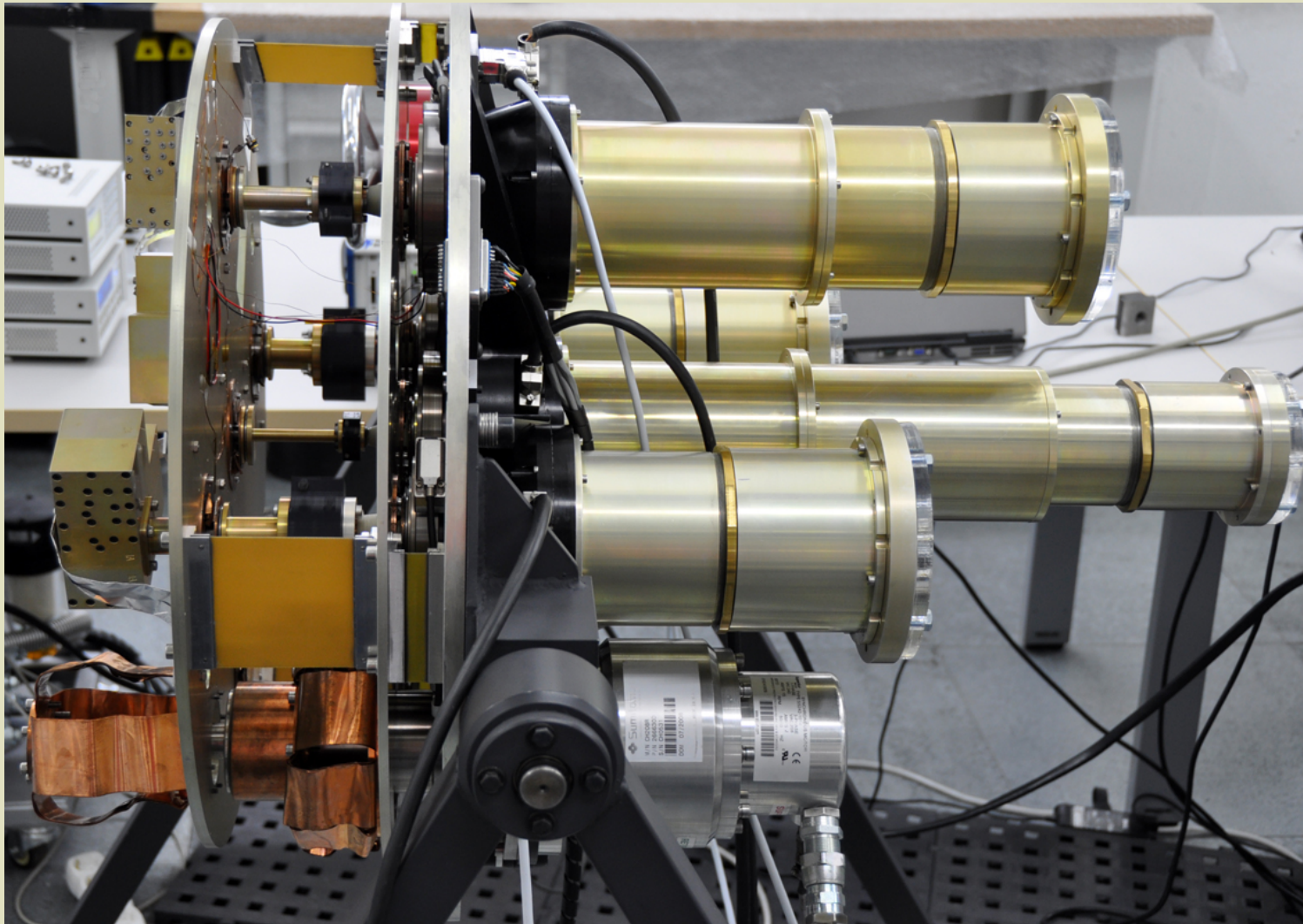


LNA
26-36 GHz

OMT
11-13 GHz

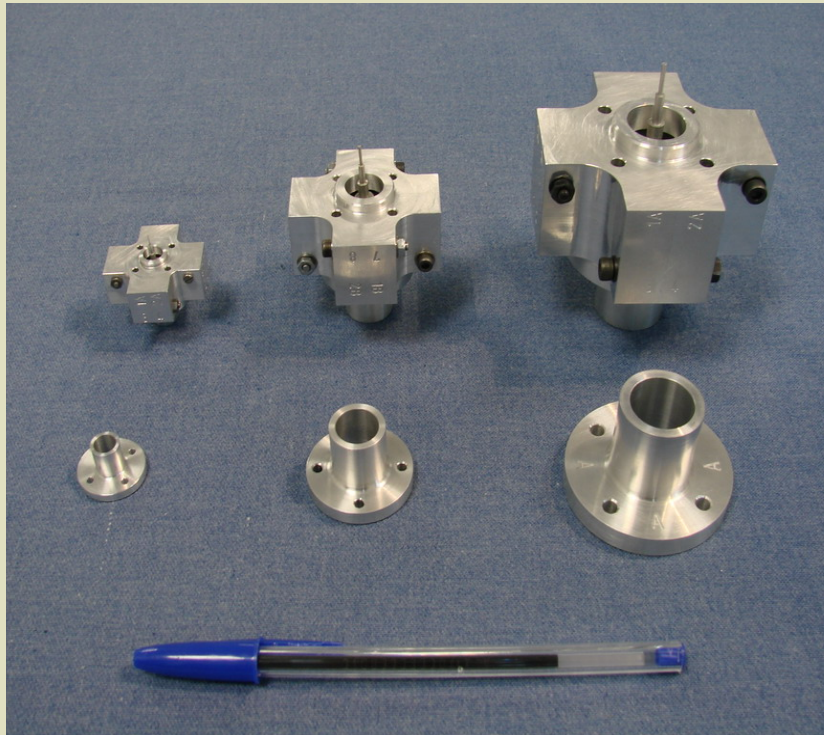
Polar
modulator
11-13 GHz





First Instrument: Four receiver chains

- Key component of the polarimeter
- Rotating polar modulator
- Cryogenically cooled: low losses, low impact on noise
- Waveguide component: turnstile 4-way junction

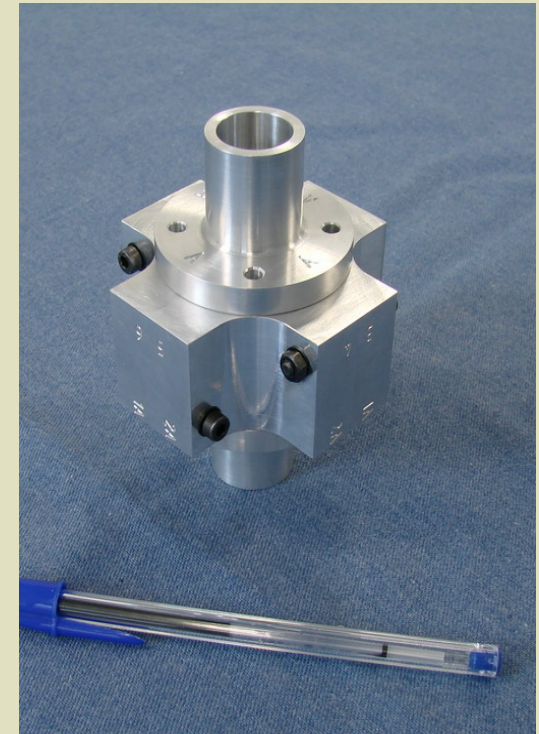


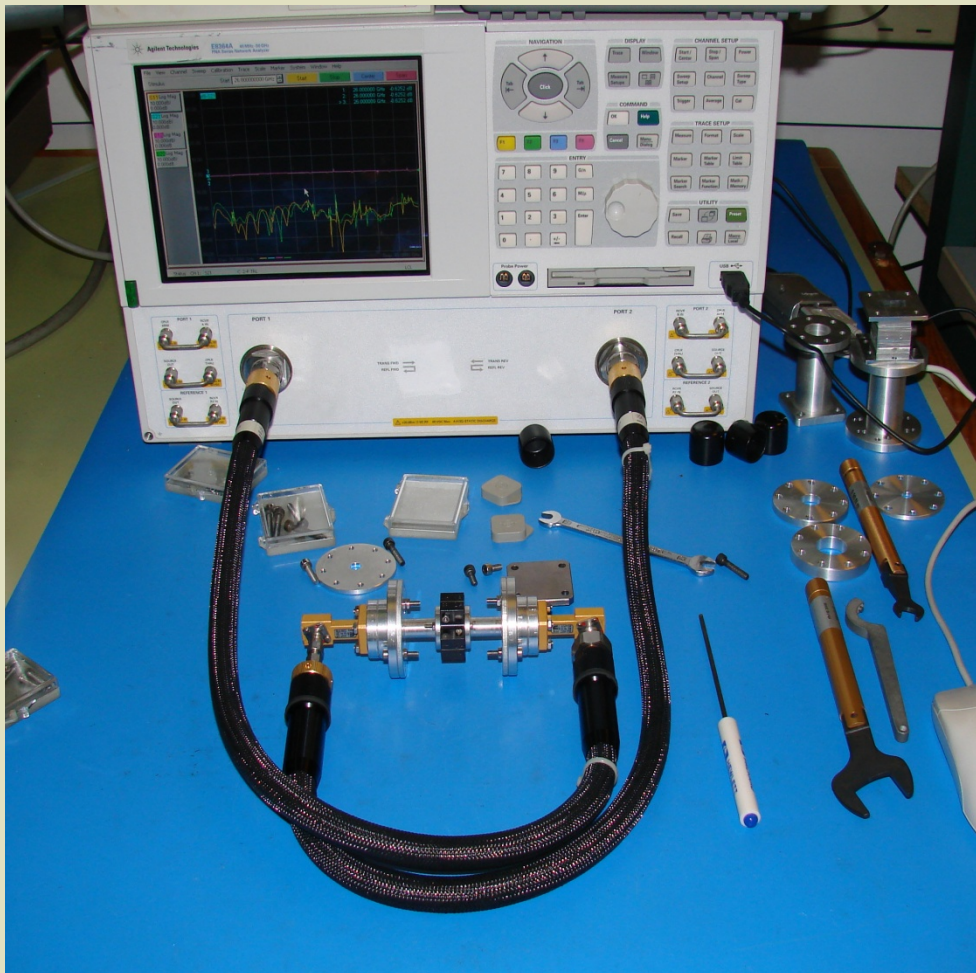
Units:

10-14 GHz

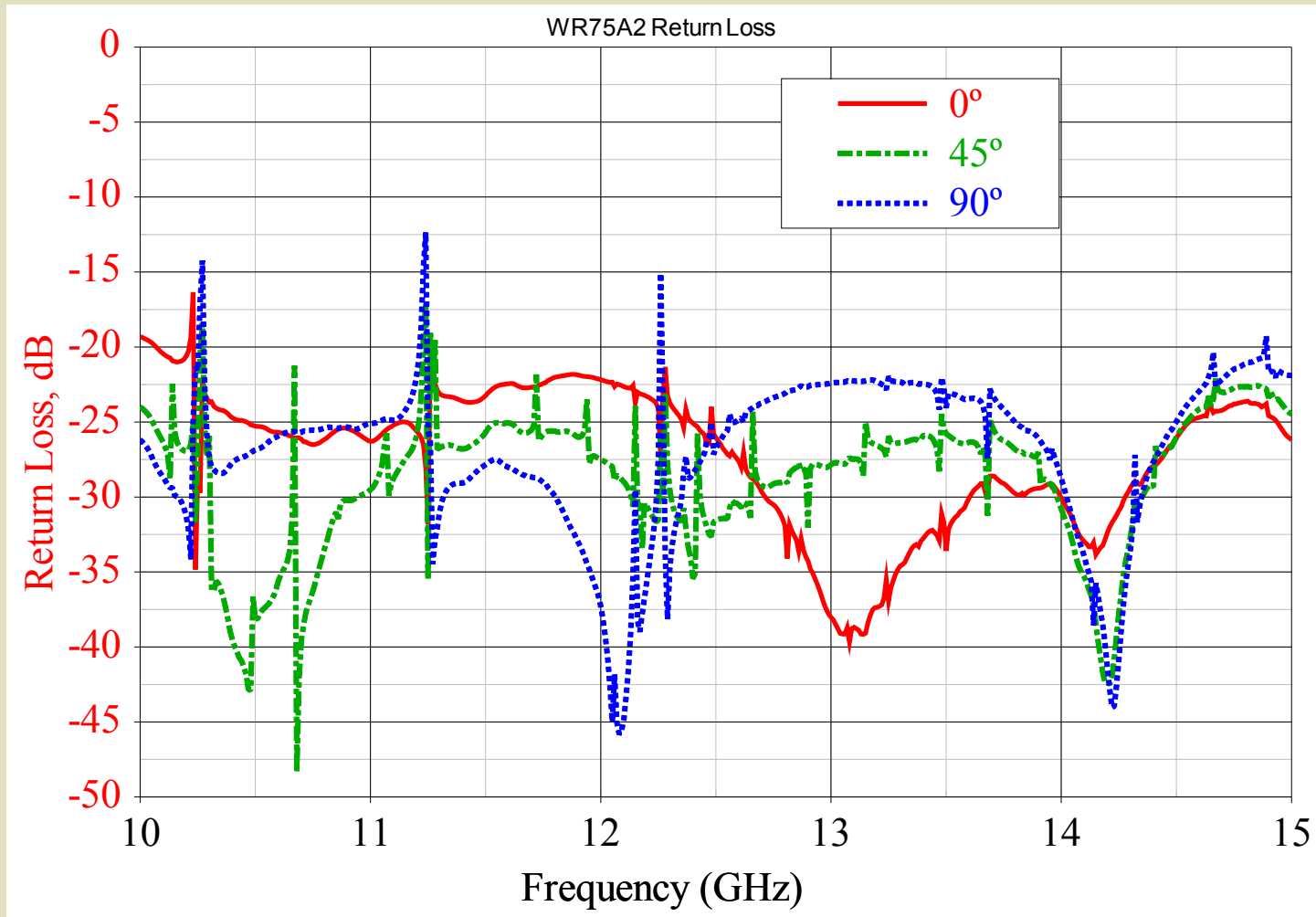
14-20 GHz

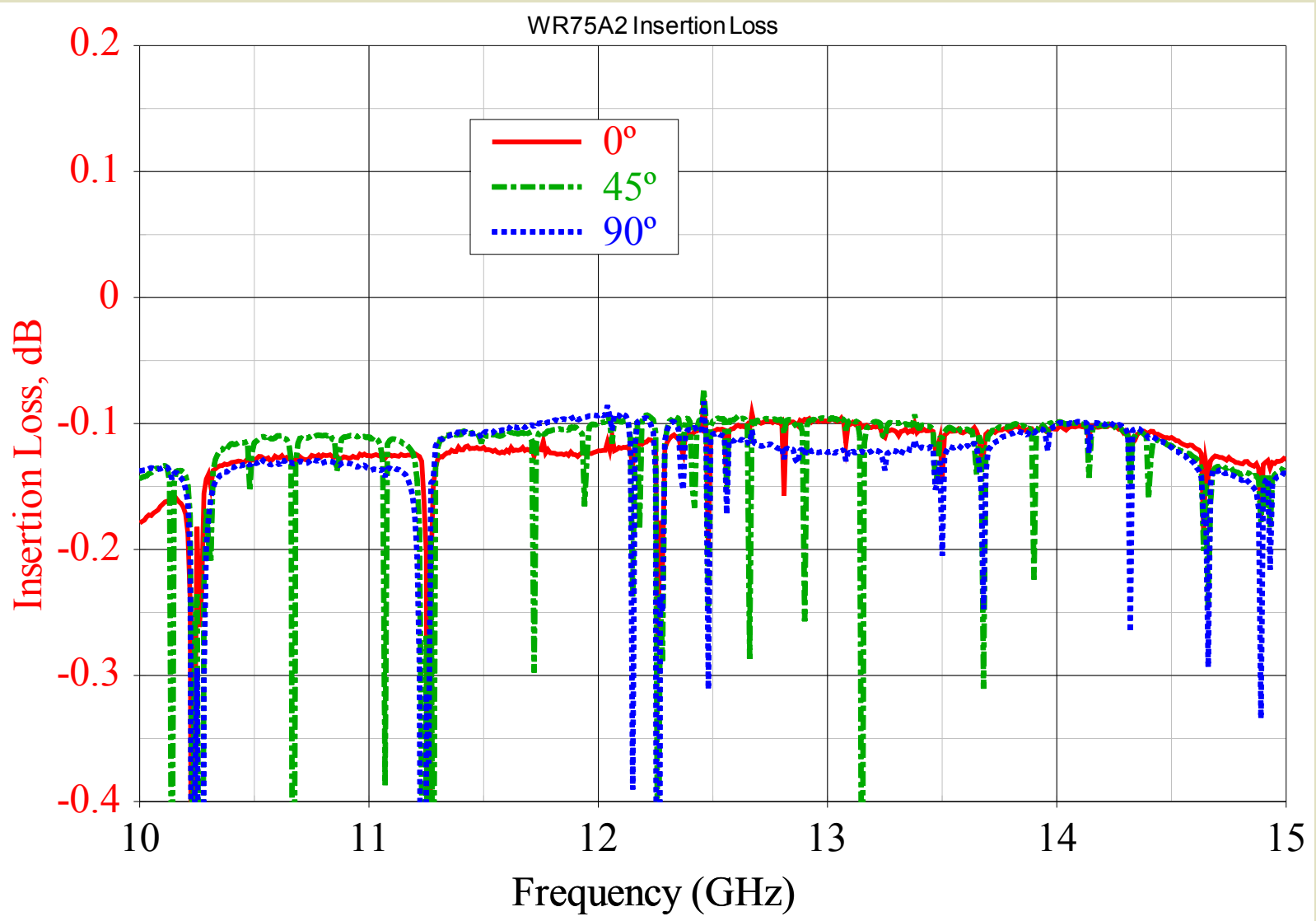
26-36 GHz

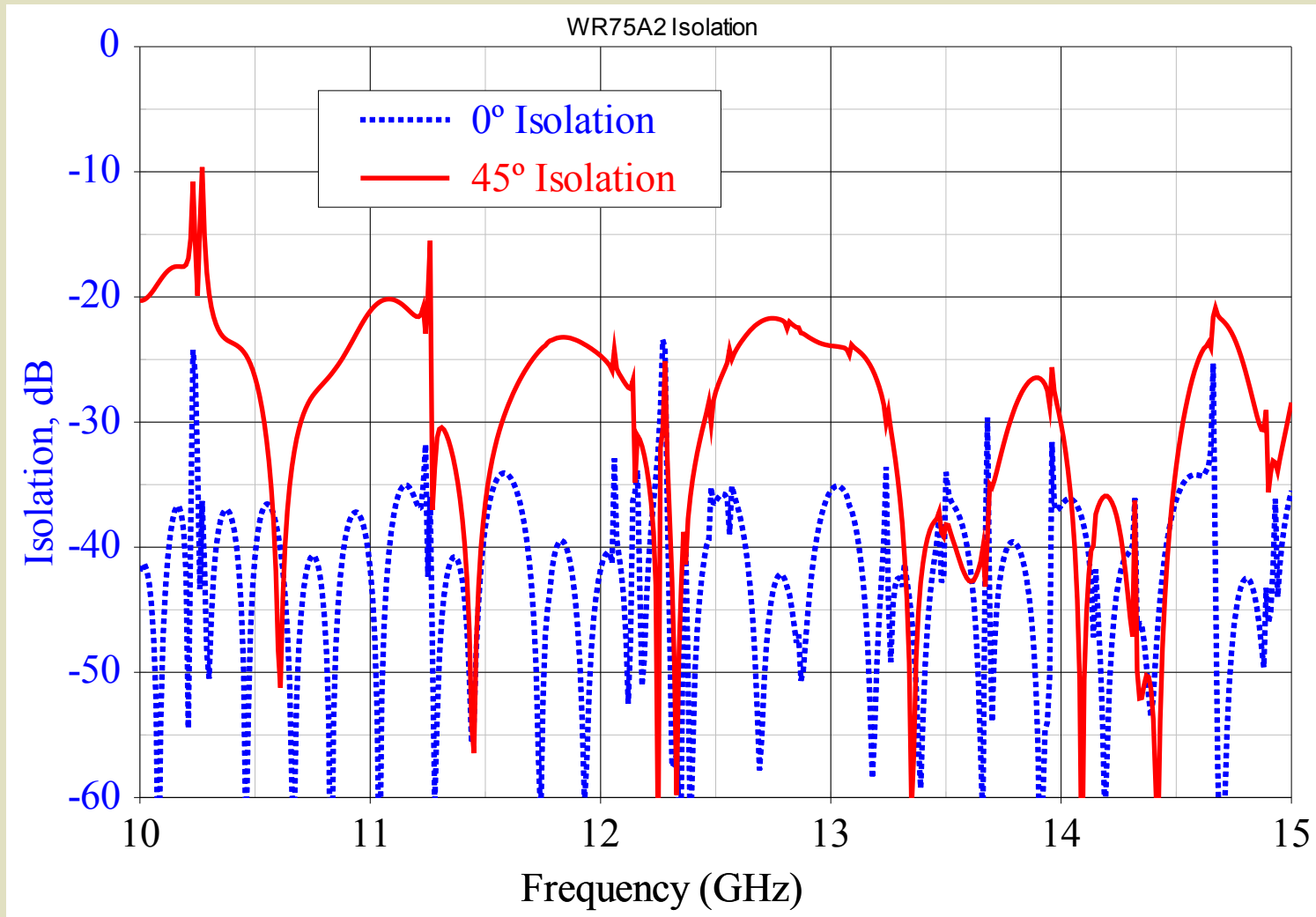




- Low return losses
- Low insertion losses
- High polar isolation
- Tests at 3 polar modulator orientations: 0° , 45° and 90°
- Plots: spikes caused by misalignment of the circular waveguide interfaces
- Tests at Room Temperature

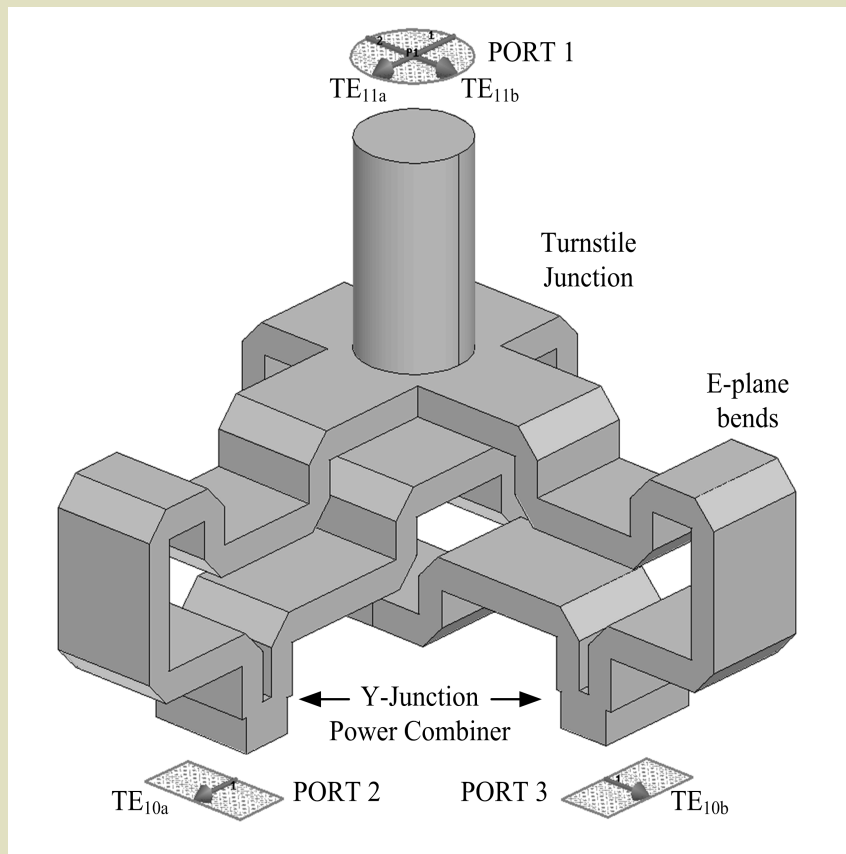




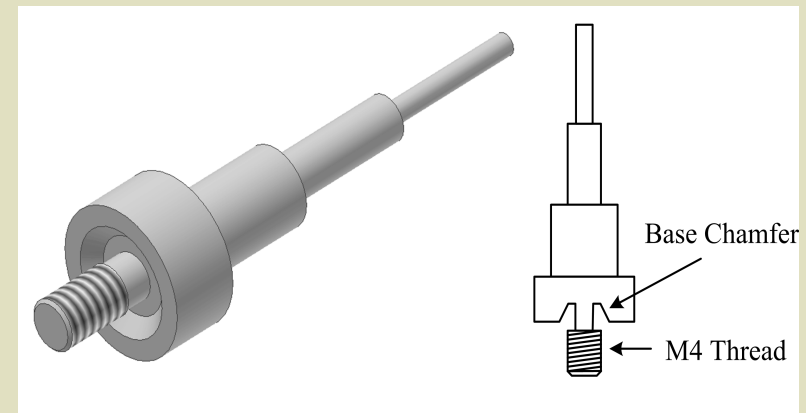
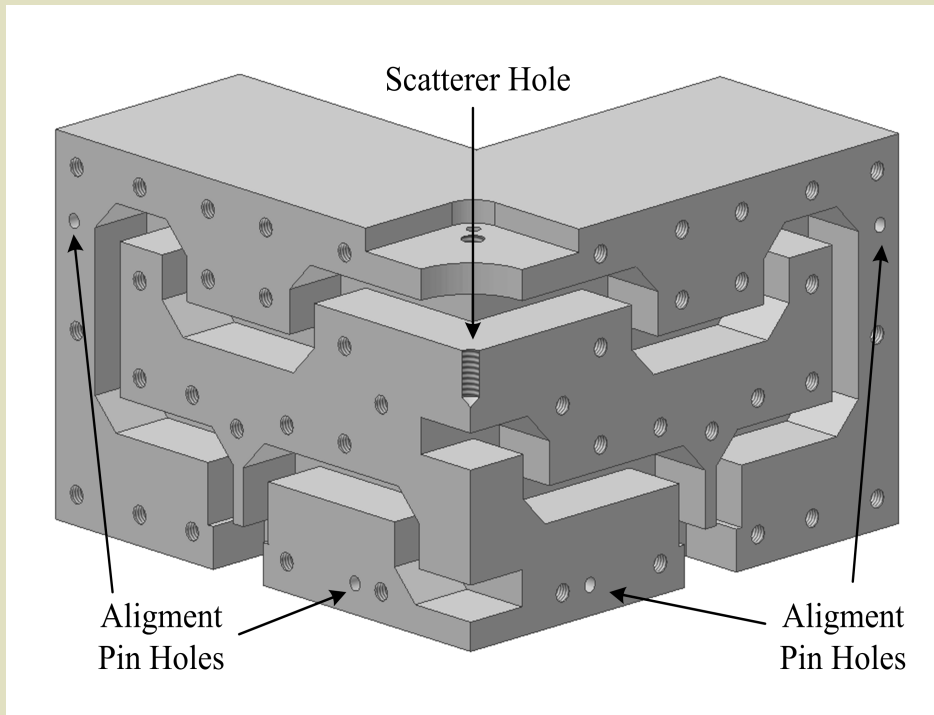


Device with physical 3-ports and electrical 4-ports

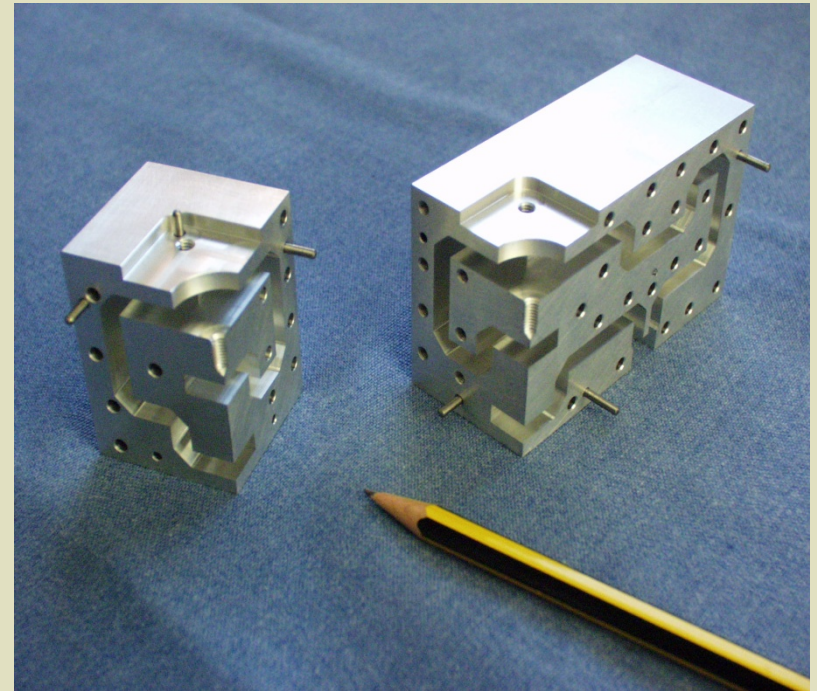
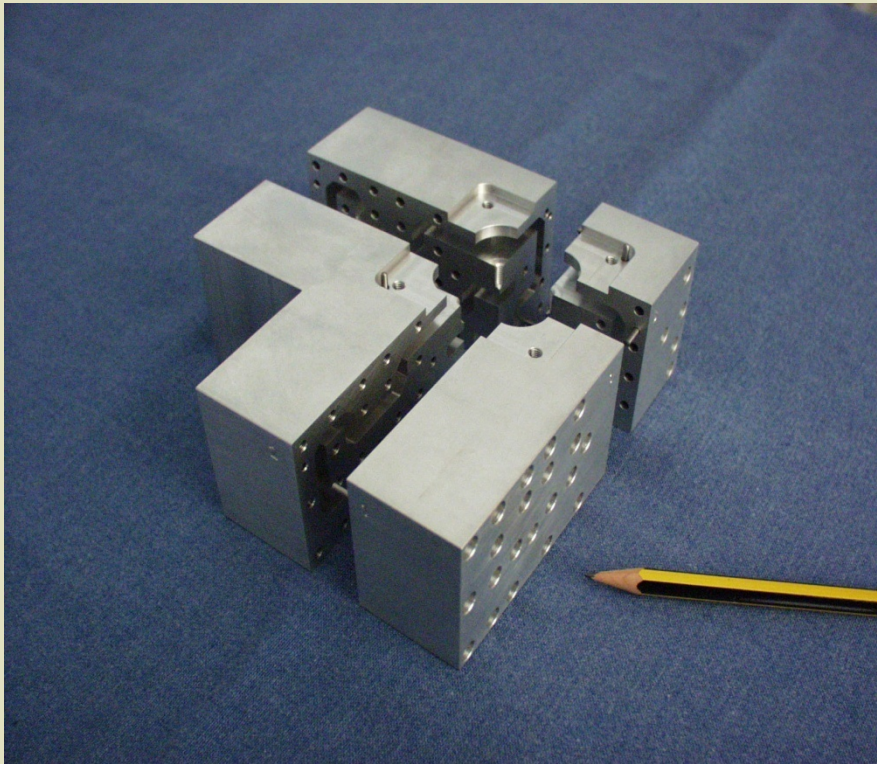
- Port 1: TE₁₀ (vertical) rectangular waveguide
- Port 2: TE₁₀ (horizontal) rectangular waveguide
- Port 3: TE₁₁ (vertical) circular waveguide
- Port 4: TE₁₁ (horizontal) circular waveguide



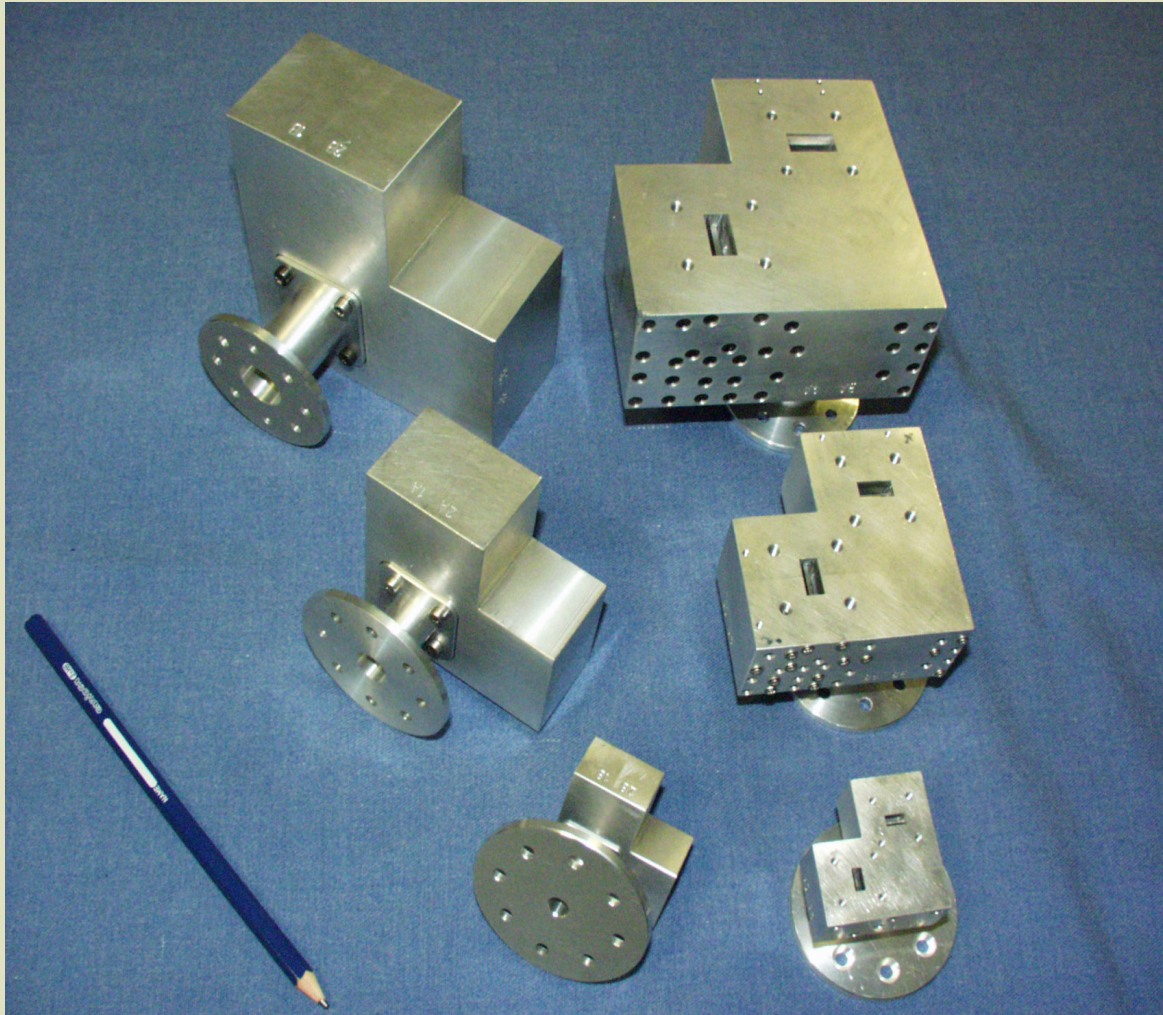
- Separates linear orthogonal polar components
- Sets a limit in the cross-polarization
- Based on turnstile junction
- Phase balanced outputs
- Broadband (> 40 % bandwidth)



- **Reduced height rectangular waveguide**
- **Optimized E-plane bends**
- **Scatterer: a critical part of turnstile junction**
- **Scalable structure (WR75, WR51, WR28)**



OMT parts (WR75 version, 10-14 GHz)

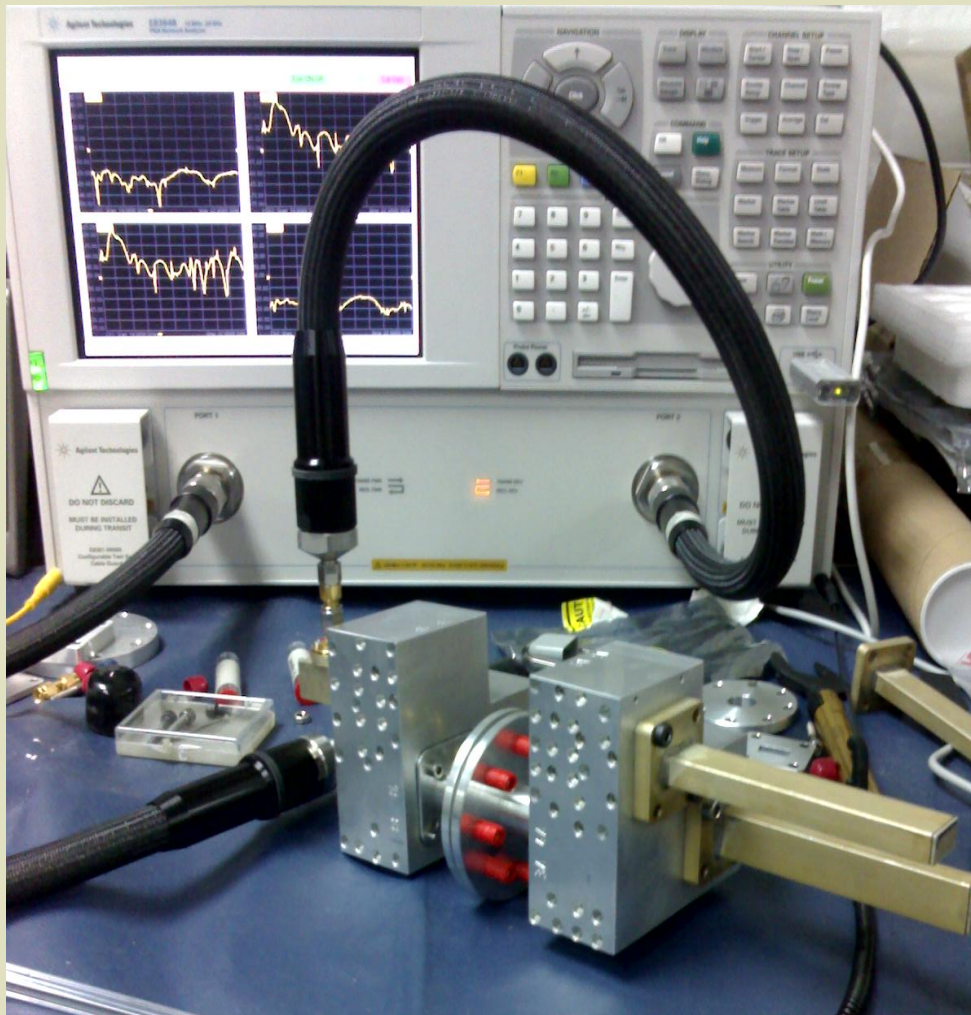


Units:

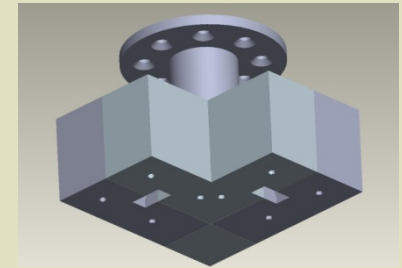
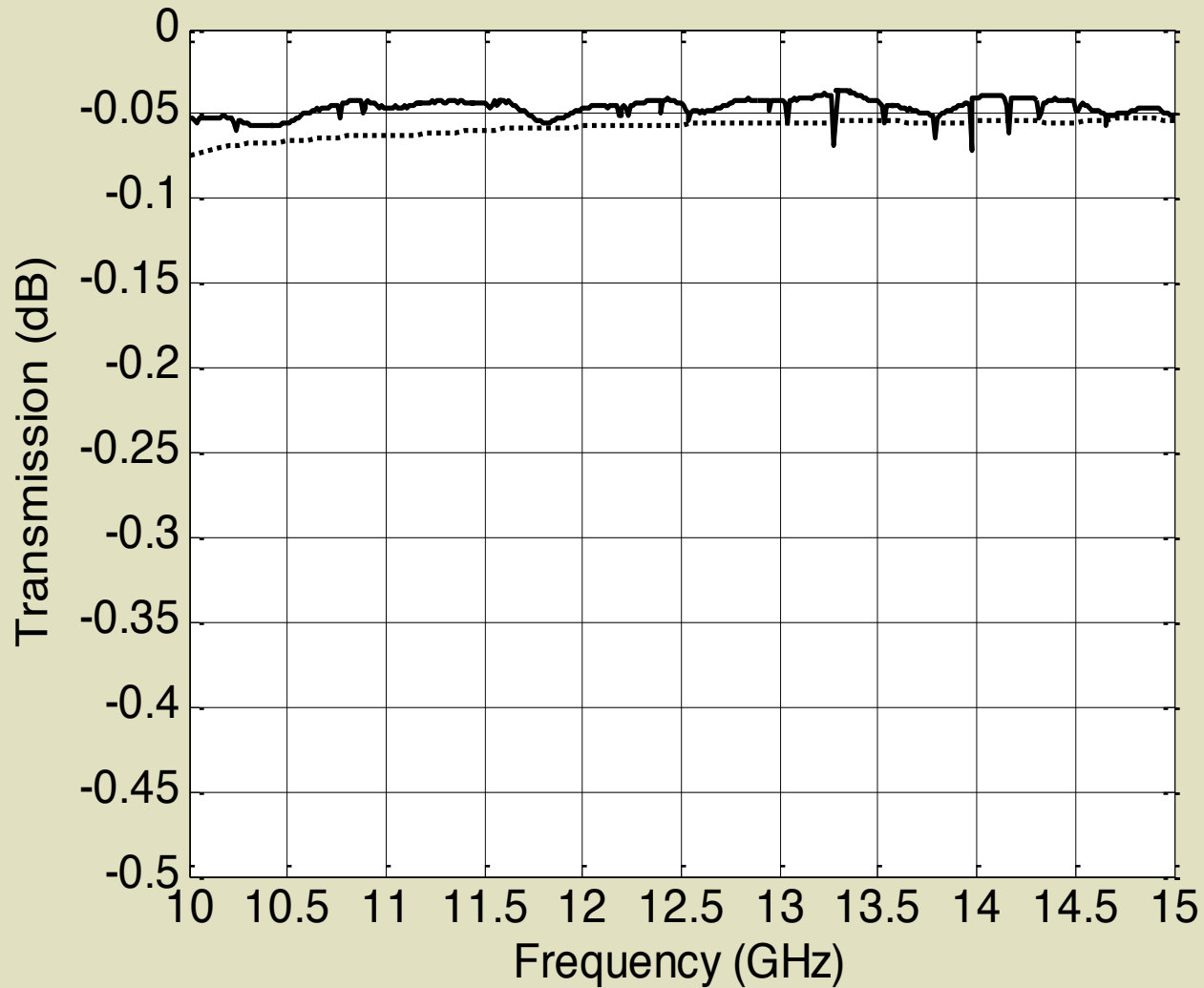
10-14 GHz

14-22 GHz

26-36 GHz



- Low return losses
- Low insertion losses
- High isolation
- Excellent phase balance
- Tests at Room Temperature

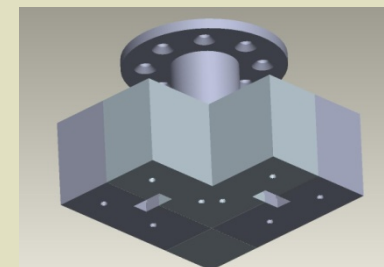
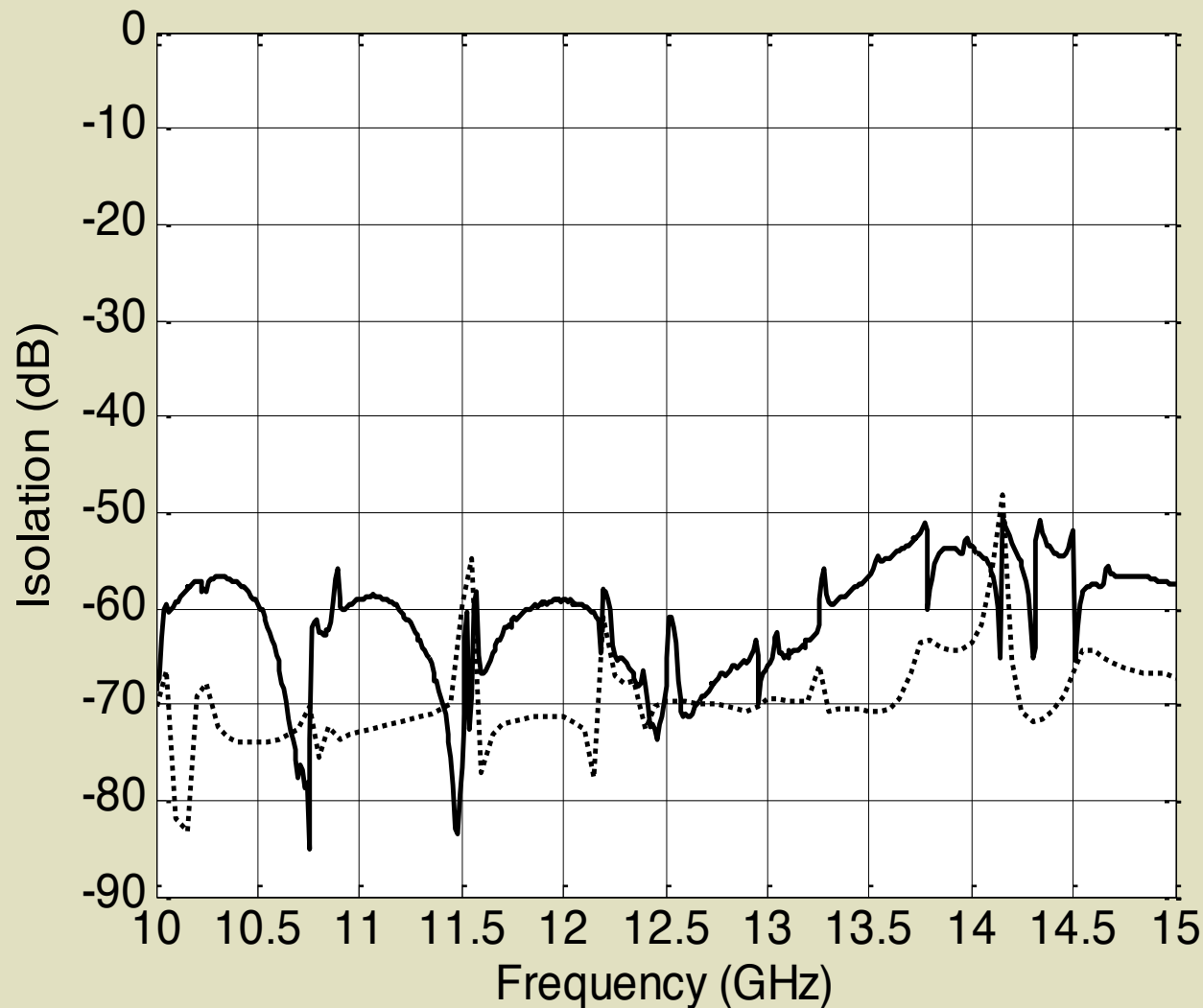


≈ 0.05 dB

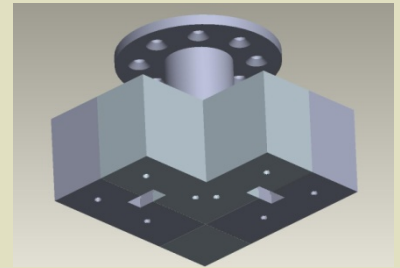
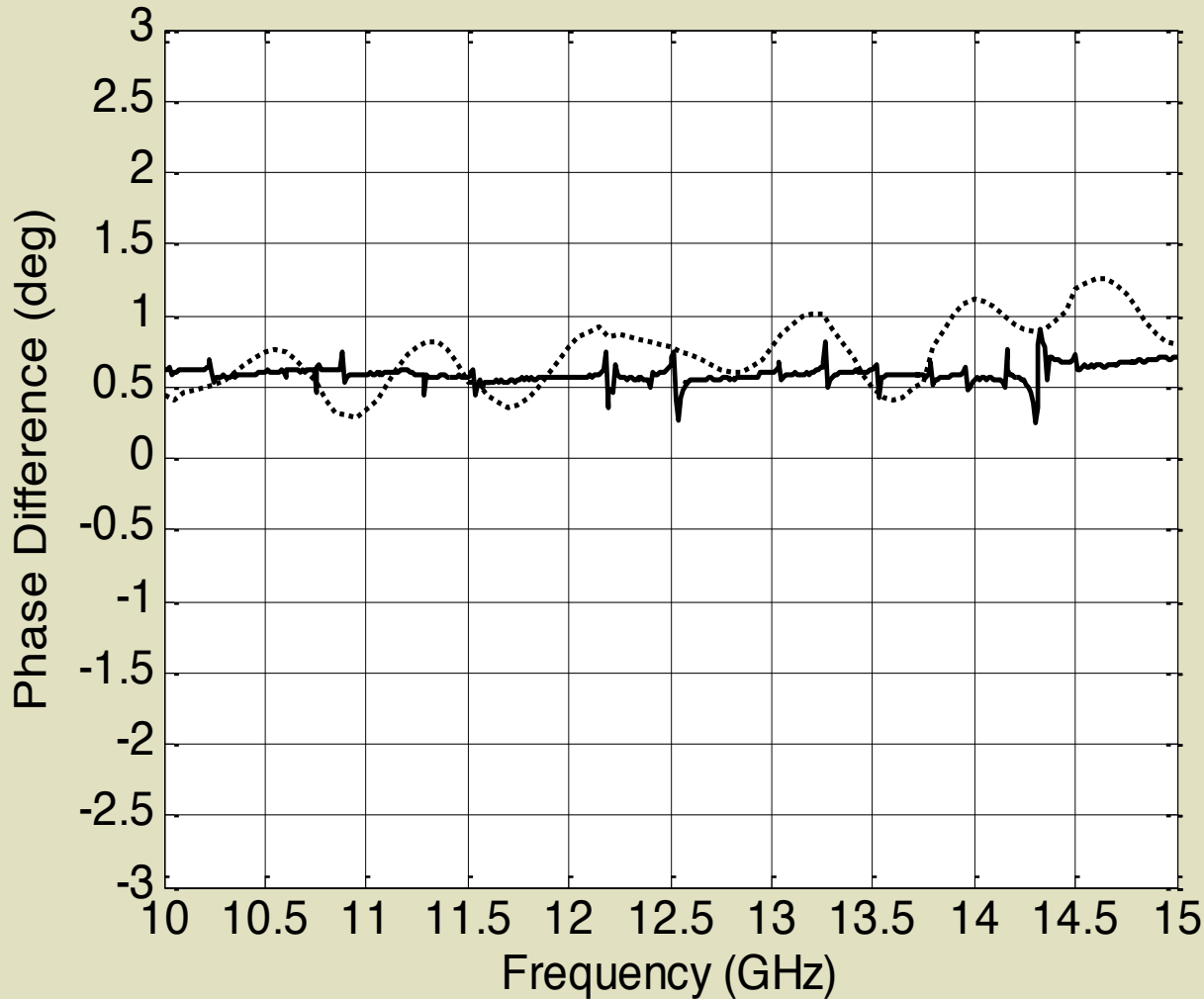
solid line: test

dashed line: simulation

OMT Isolation (between rectangular ports)

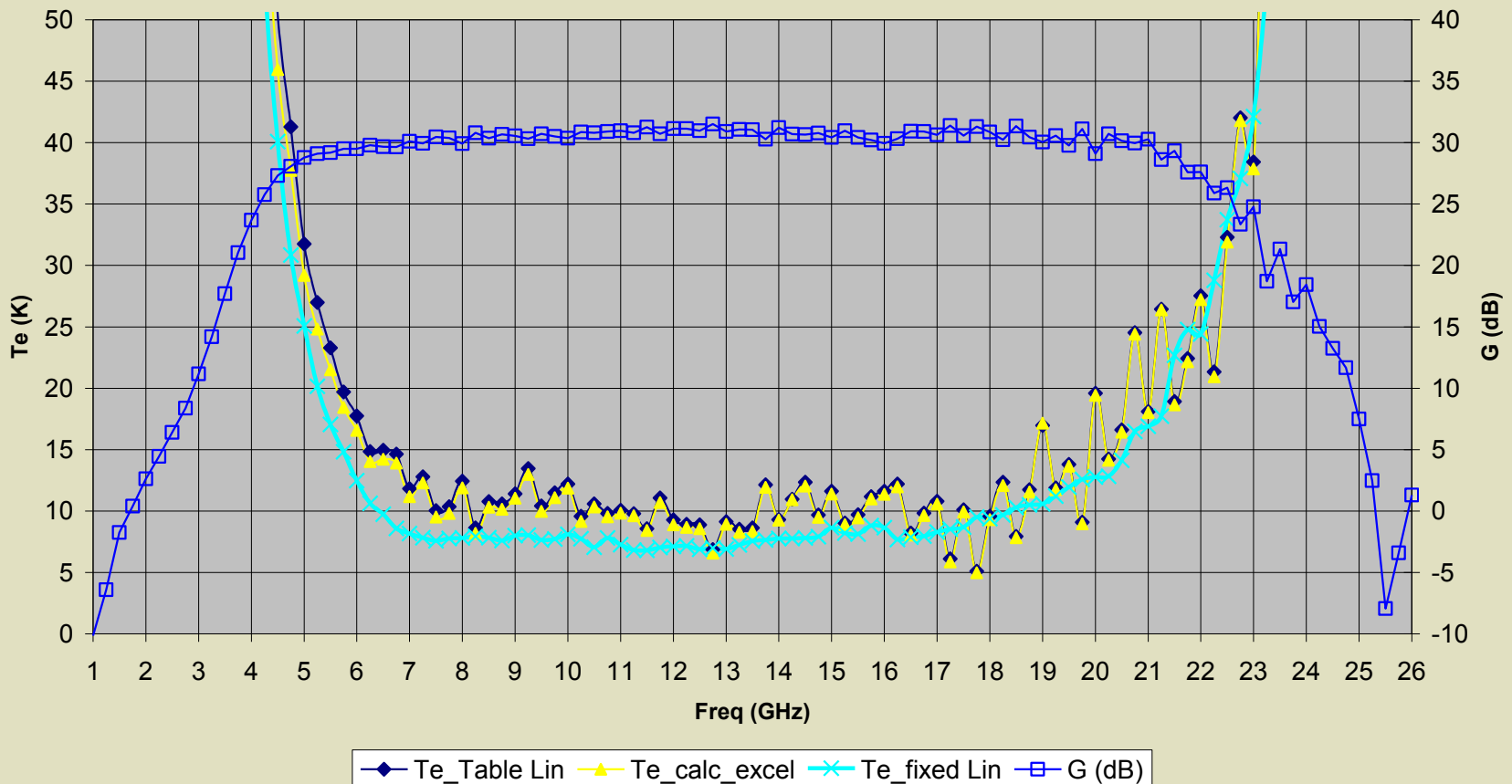


better than 50 dB

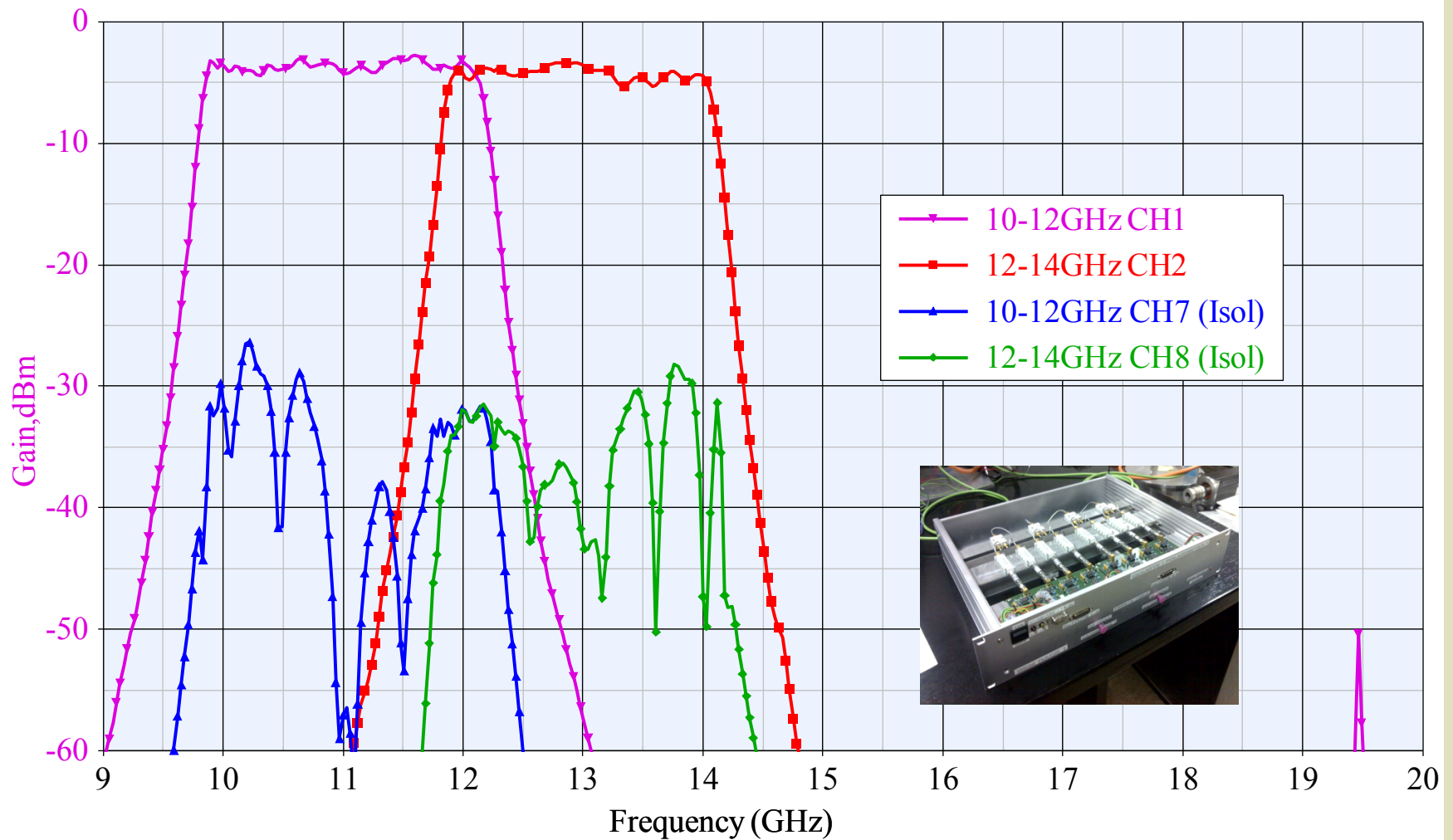


$\Delta\text{phase} < 0.7^\circ$

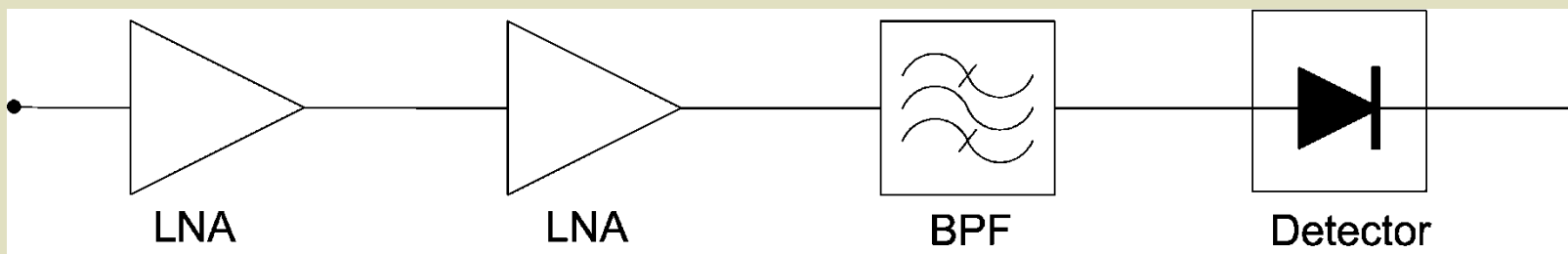
LNA #40A28 24K 290208
 Vg1=1V Vg2=1V Vd=0.65V Id=16mA
 NFA 8975A Loss Comp. Table T_input=22.9K



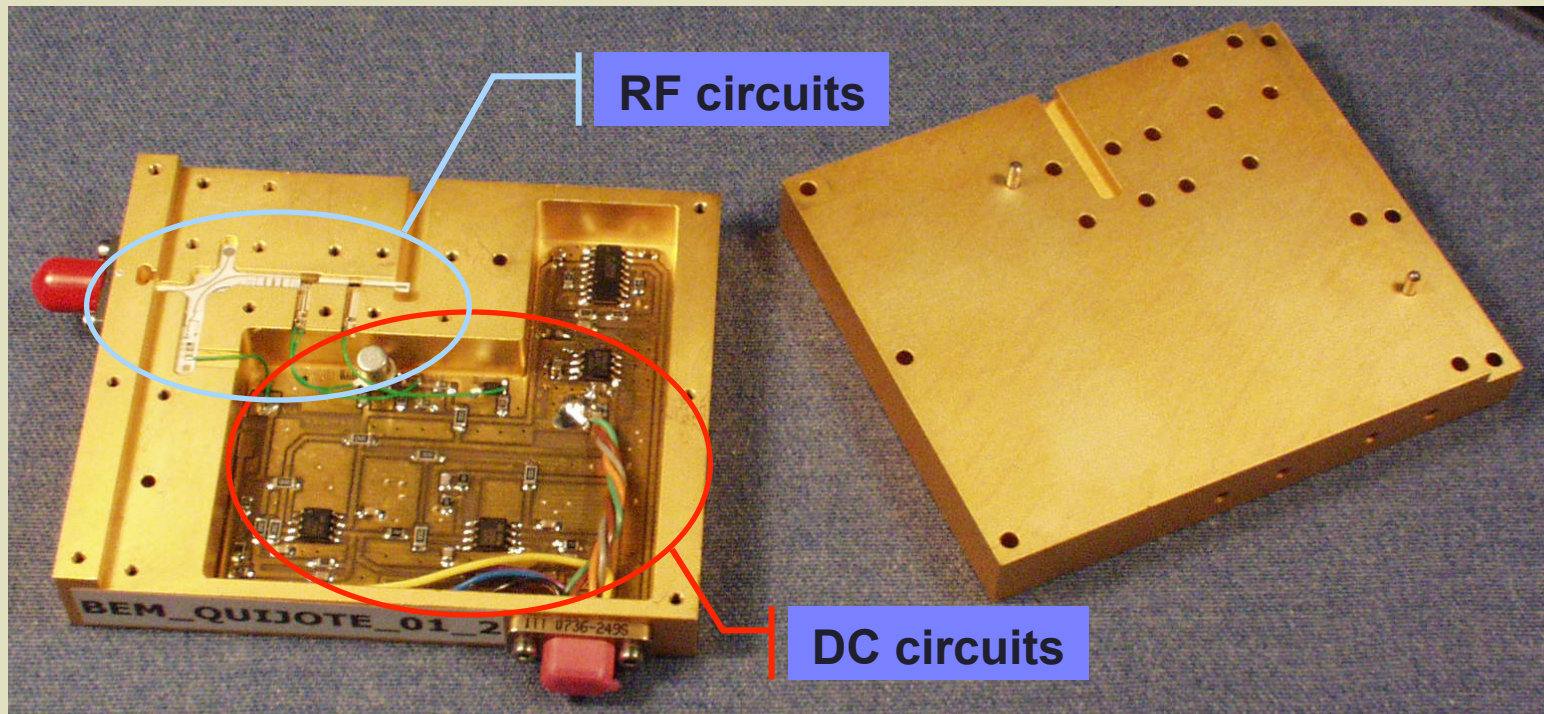
LNA for low frequency channels



One branch
30 GHz BEM Block diagram
(180° hybrid and video amp not included)

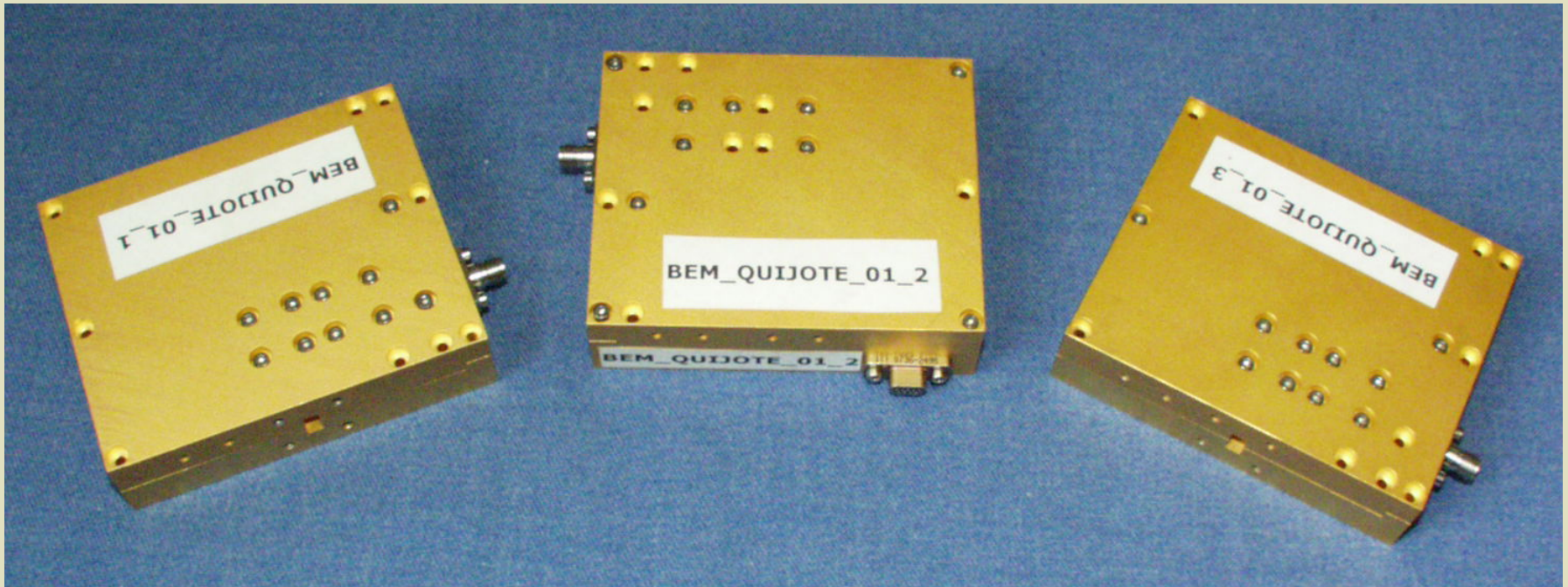


Bandwidth: 26 to 36 GHz
Noise temperature < 500 K

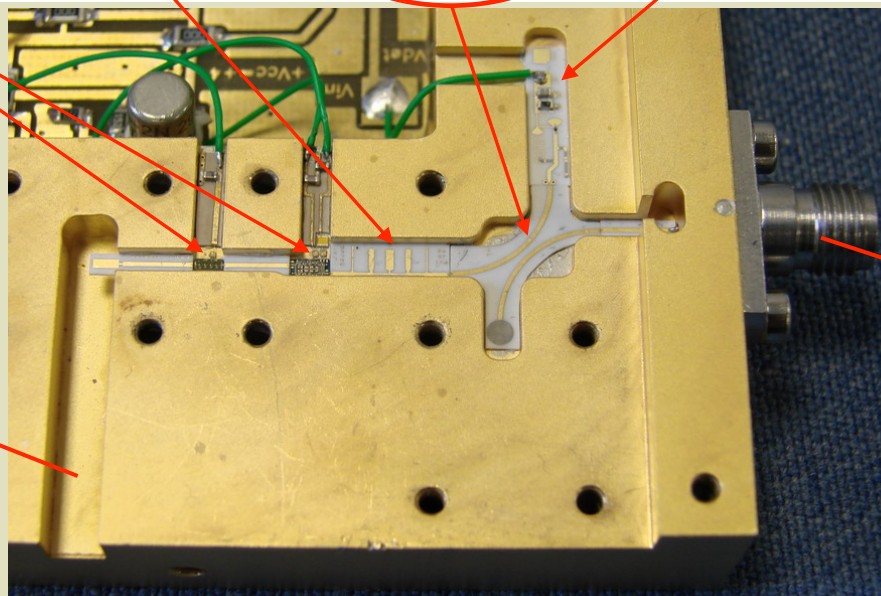
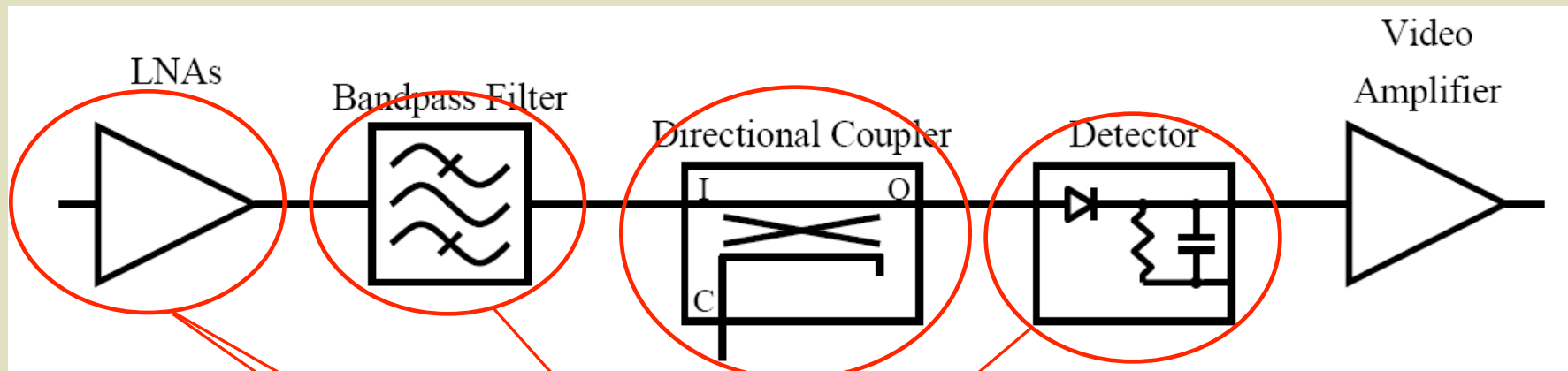


BEM branch (top cover removed)

Manufactured BEM units: 2 + 1 (spare)

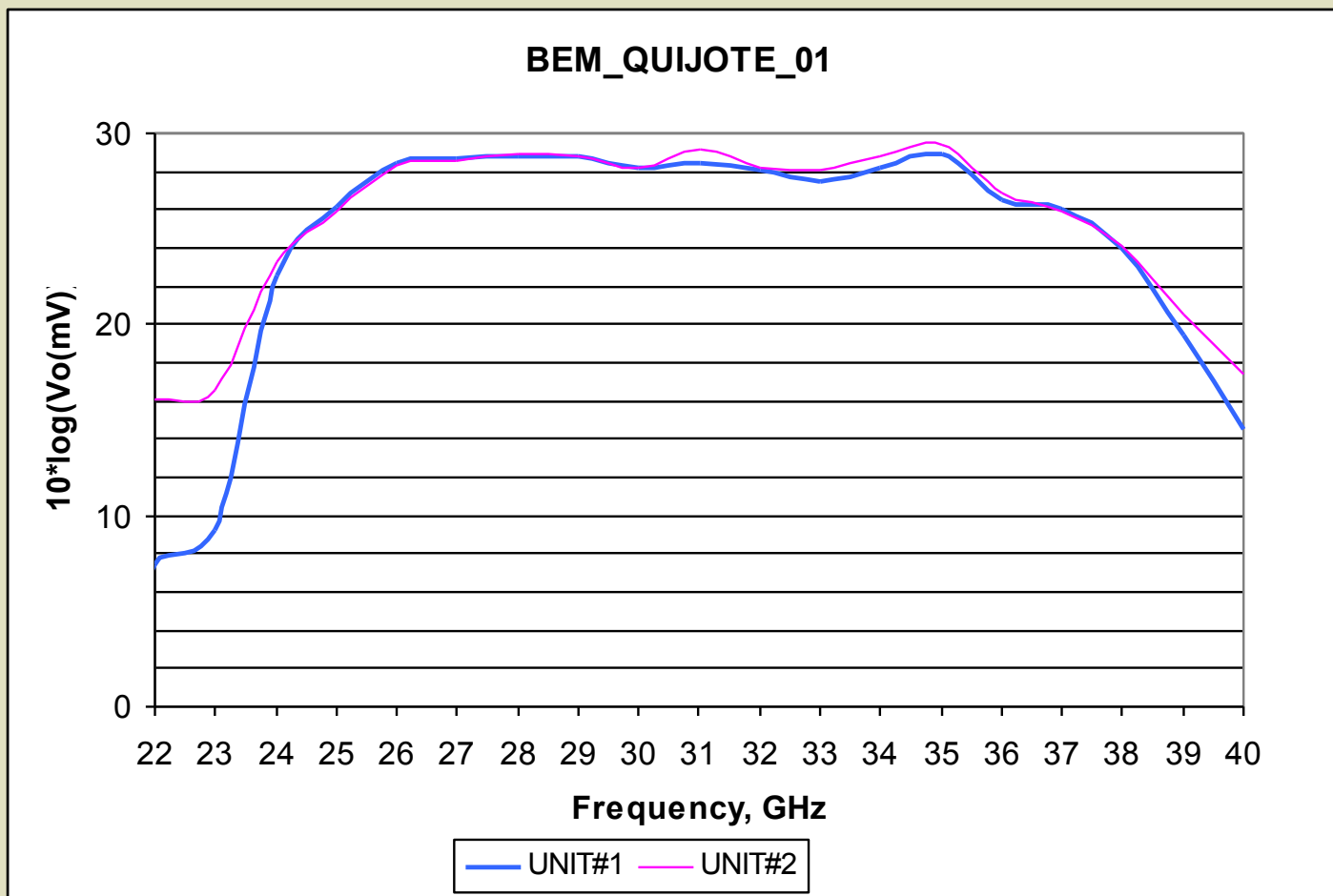


Original prototype without 180° hybrids



Waveguide
input

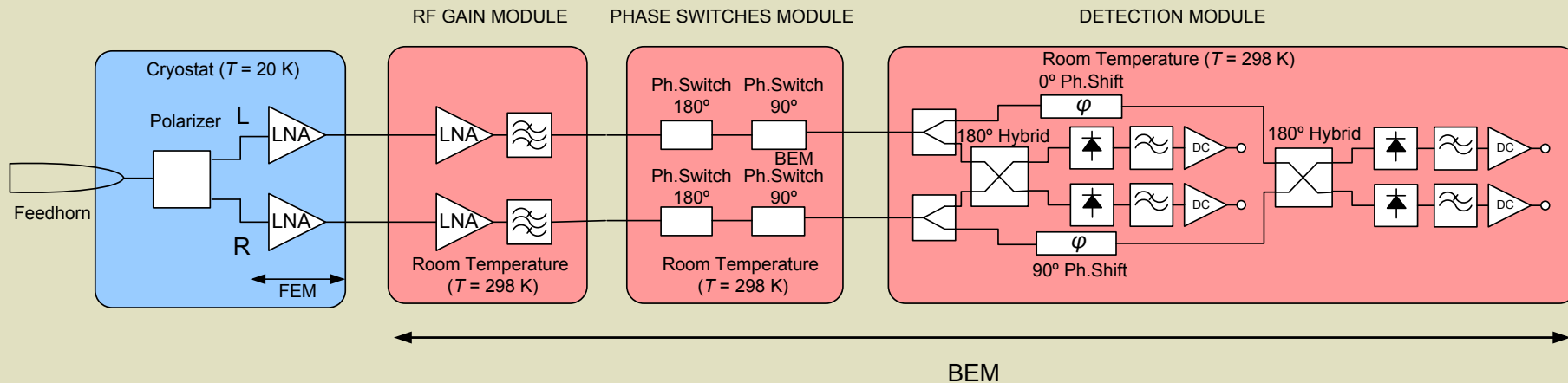
RF sample
output (K
connector)



Gain vs. frequency for two units (detector included)

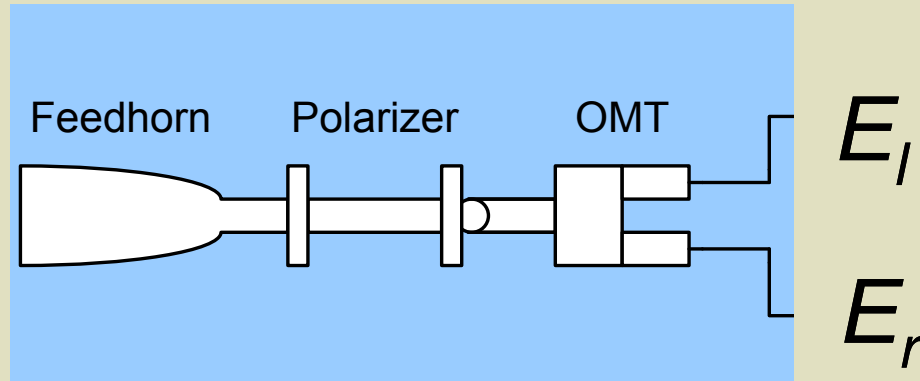


Frontal panel of 30 GHz BEM rack



New receiver scheme:

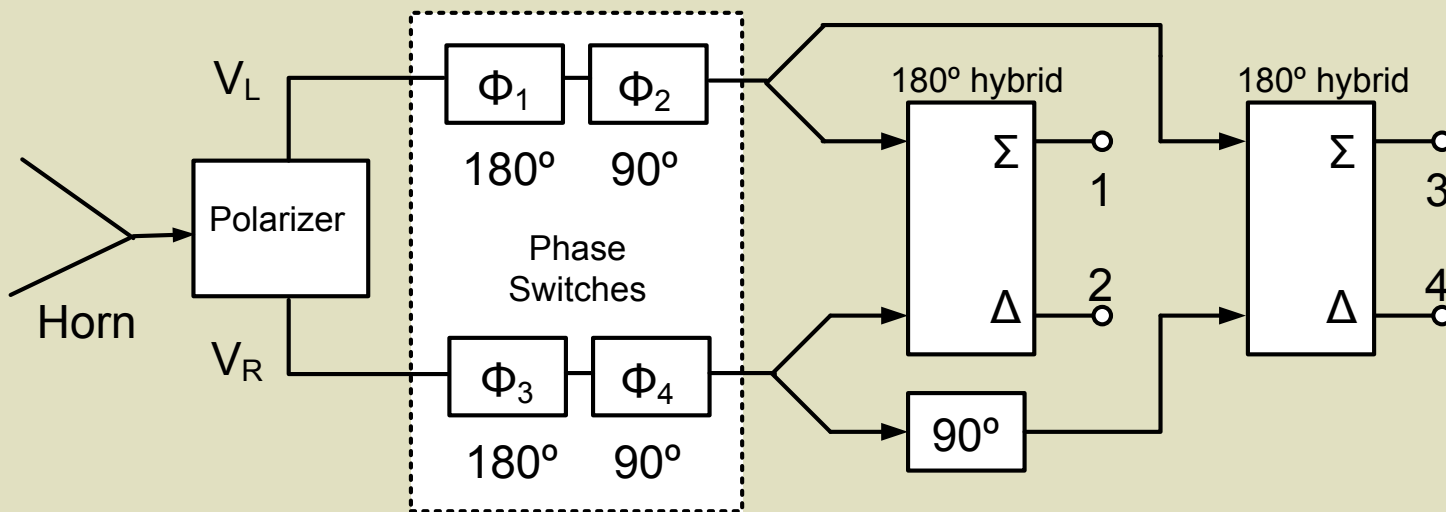
- electronic phase switching in two balanced branches
- microwave correlation (180° hybrid)
- direct detection (Schottky diode)



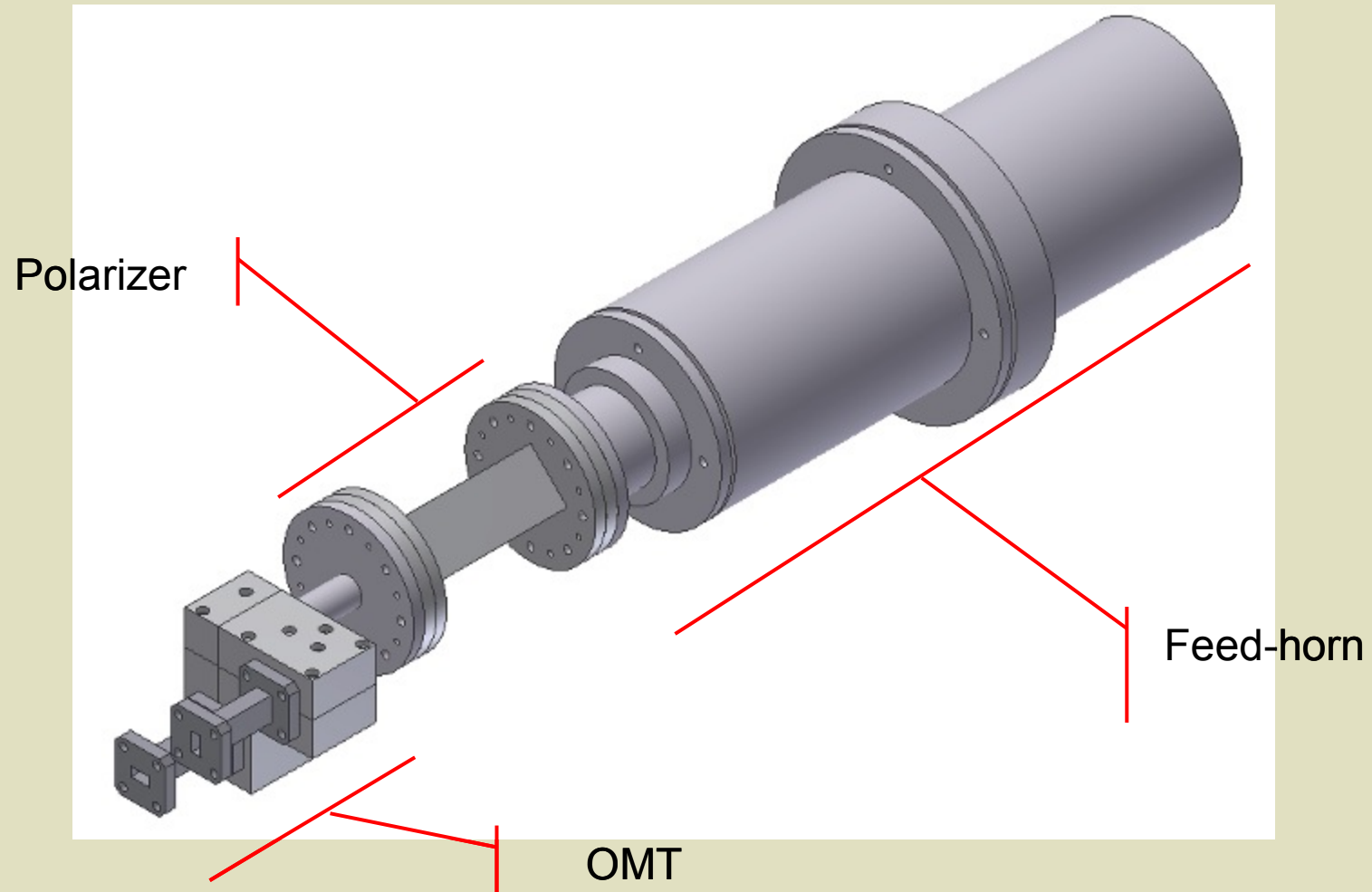
Circular components of electric fields

$$\begin{pmatrix} I \\ Q \\ U \end{pmatrix} \equiv \begin{pmatrix} |E_l|^2 + |E_r|^2 \\ 2 \operatorname{Re}(E_l^* E_r) \\ -2 \operatorname{Im}(E_l^* E_r) \end{pmatrix}$$

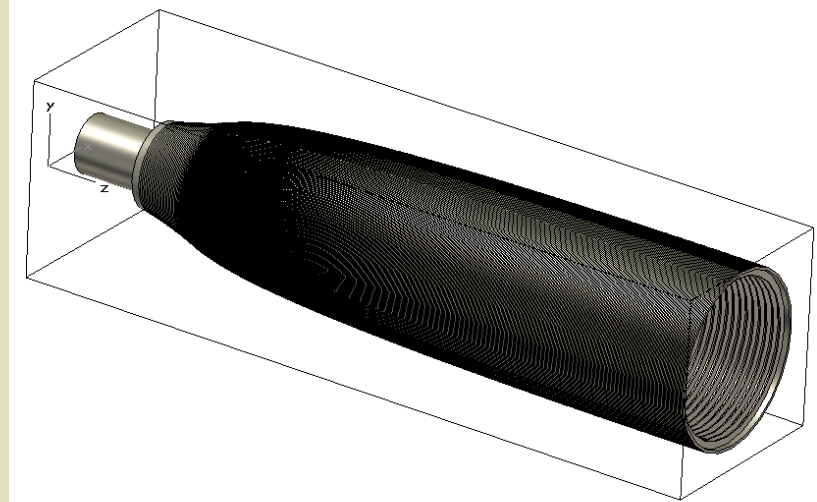
Stokes parameters



Φ	I	Q	U
0°	$V_{d1} + V_{d2} = V_{d3} + V_{d4}$	$V_{d1} - V_{d2}$	$V_{d3} - V_{d4}$
90°	$V_{d1} + V_{d2} = V_{d3} + V_{d4}$	$V_{d3} - V_{d4}$	$V_{d2} - V_{d1}$
180°	$V_{d1} + V_{d2} = V_{d3} + V_{d4}$	$V_{d2} - V_{d1}$	$V_{d4} - V_{d3}$
270°	$V_{d1} + V_{d2} = V_{d3} + V_{d4}$	$V_{d4} - V_{d3}$	$V_{d1} - V_{d2}$



3D model for EM simulations

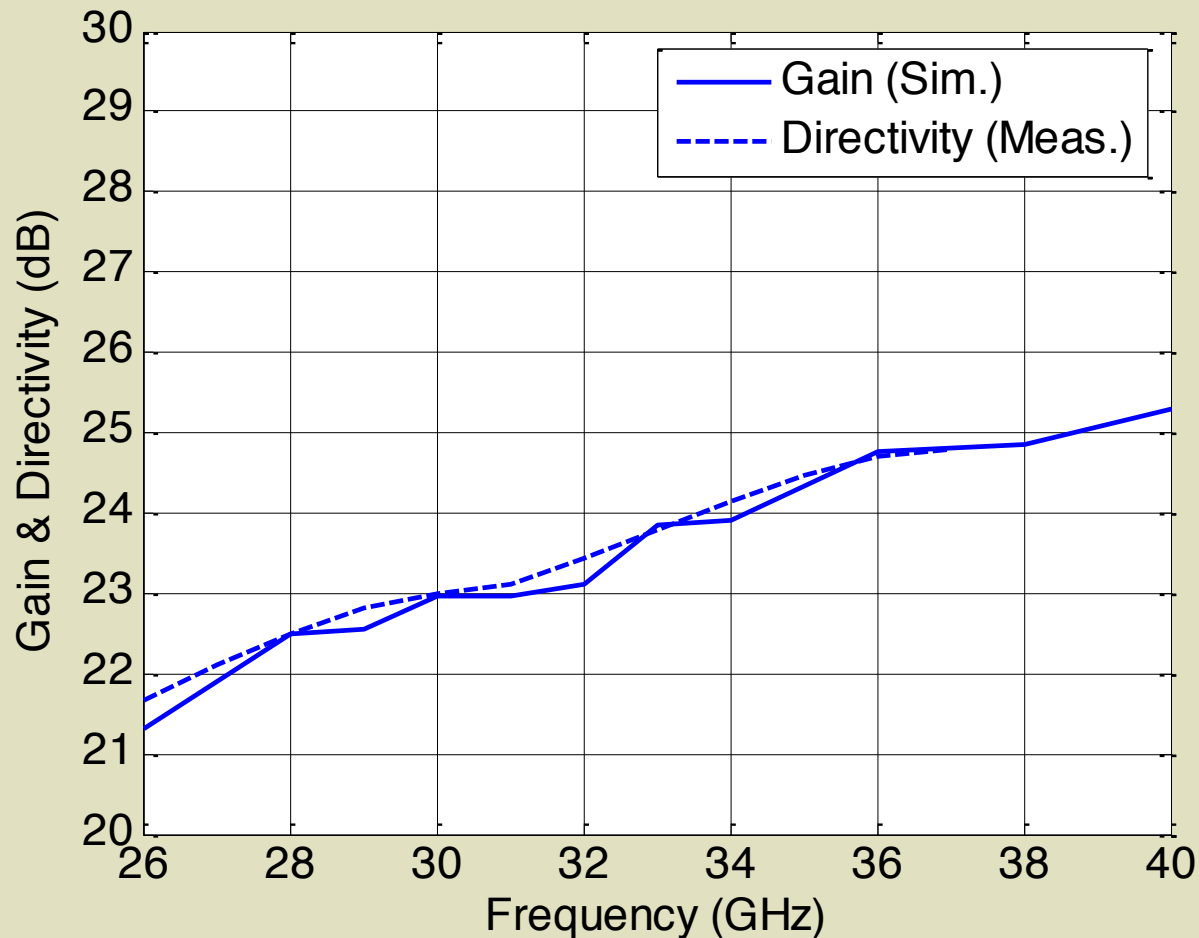


Feed-horn prototype

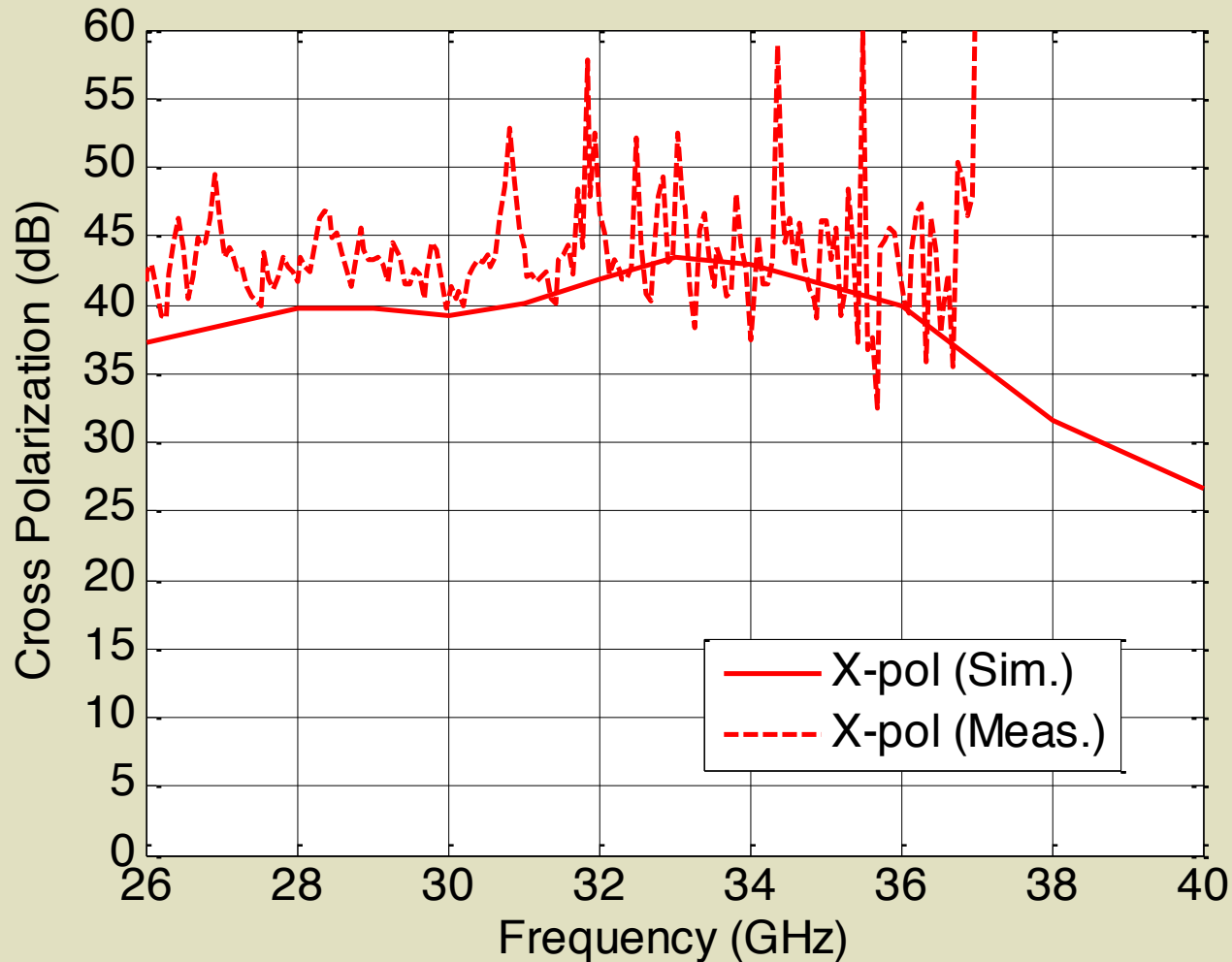


Feed-horn directivity measurements

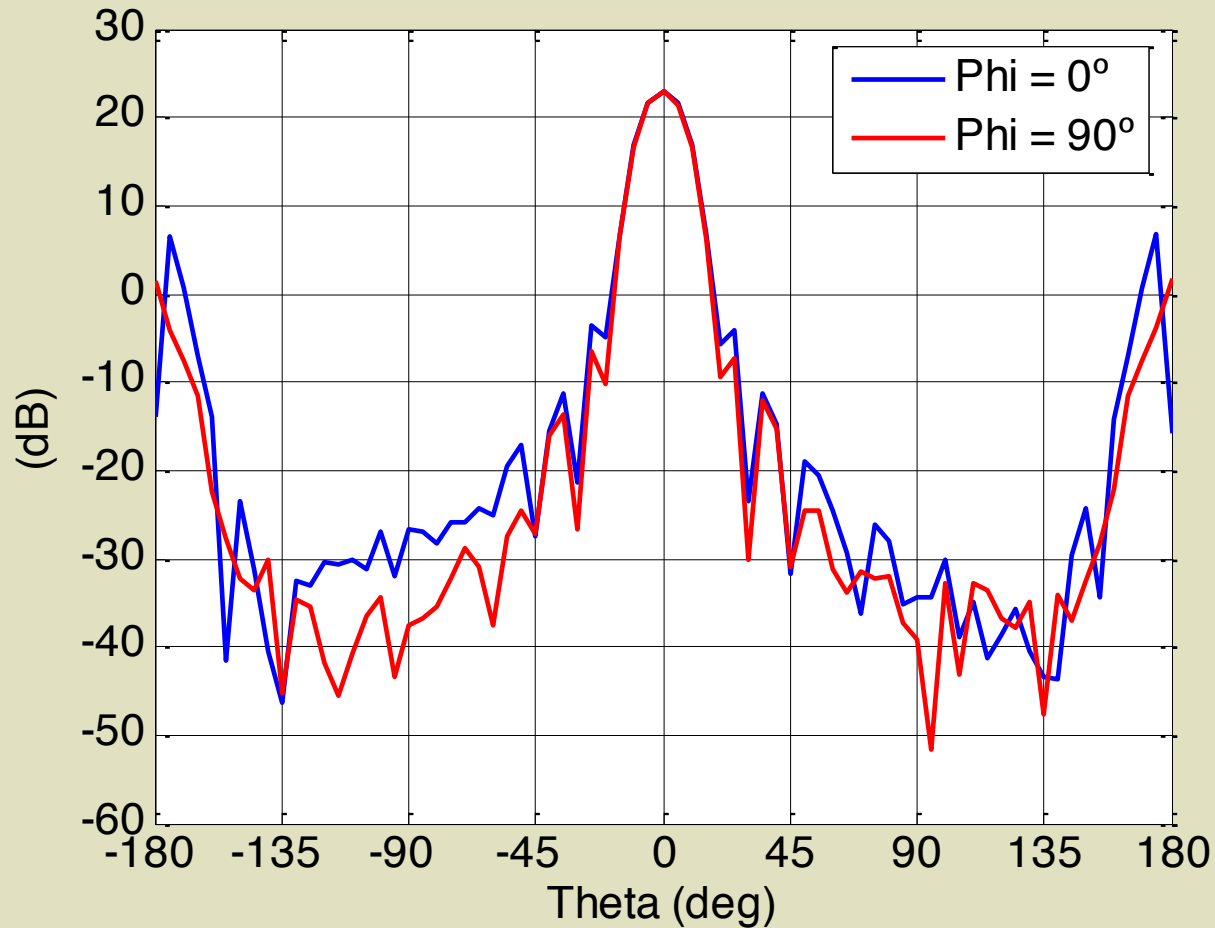
Feed-horn losses not included. (Loss < 0.5 dB)



Feed-horn cross-polarization measurements

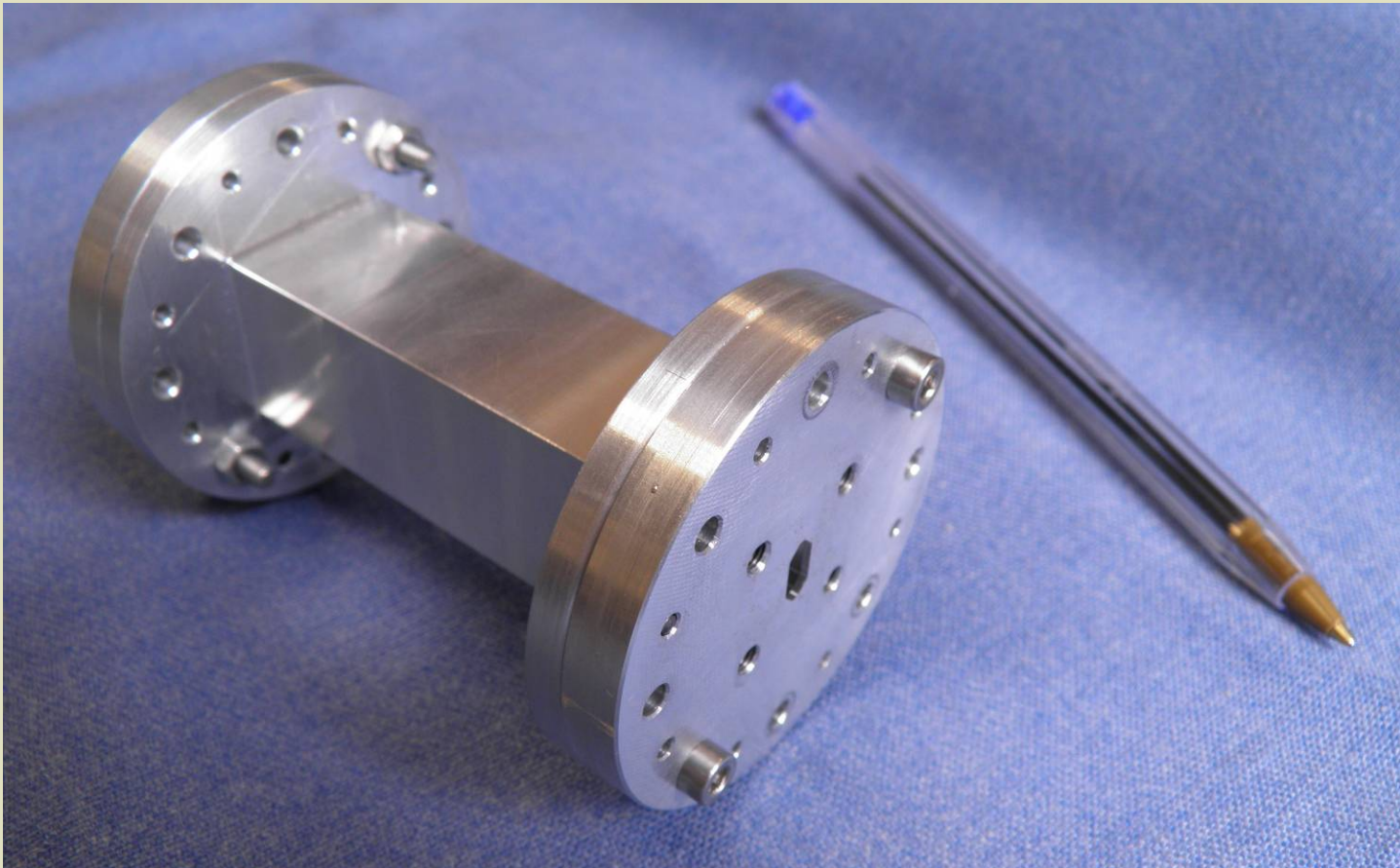


Feed-horn radiation-pattern measurements (at 32 GHz)



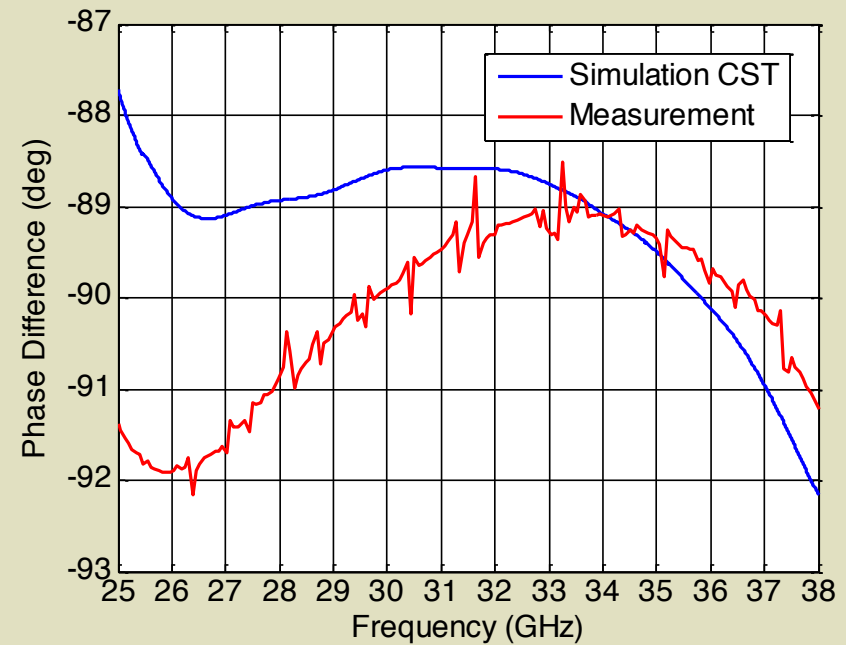
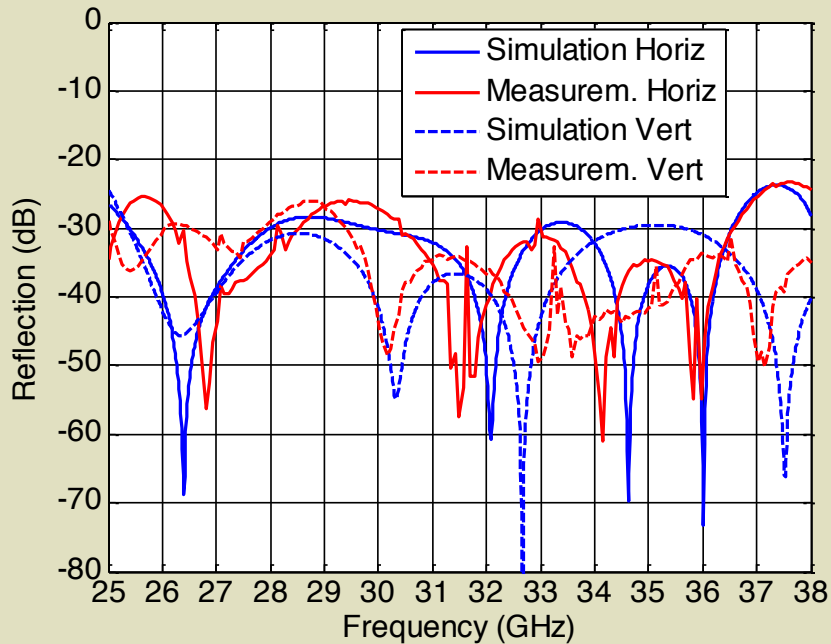
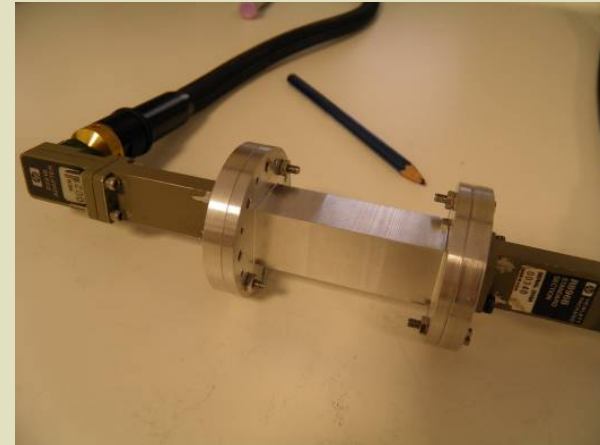
Polarizer (26-36 GHz)

Square waveguide component (internal corrugations)
90° differential phase shift (TE_{10} and TE_{01} orthogonal modes)



Test results

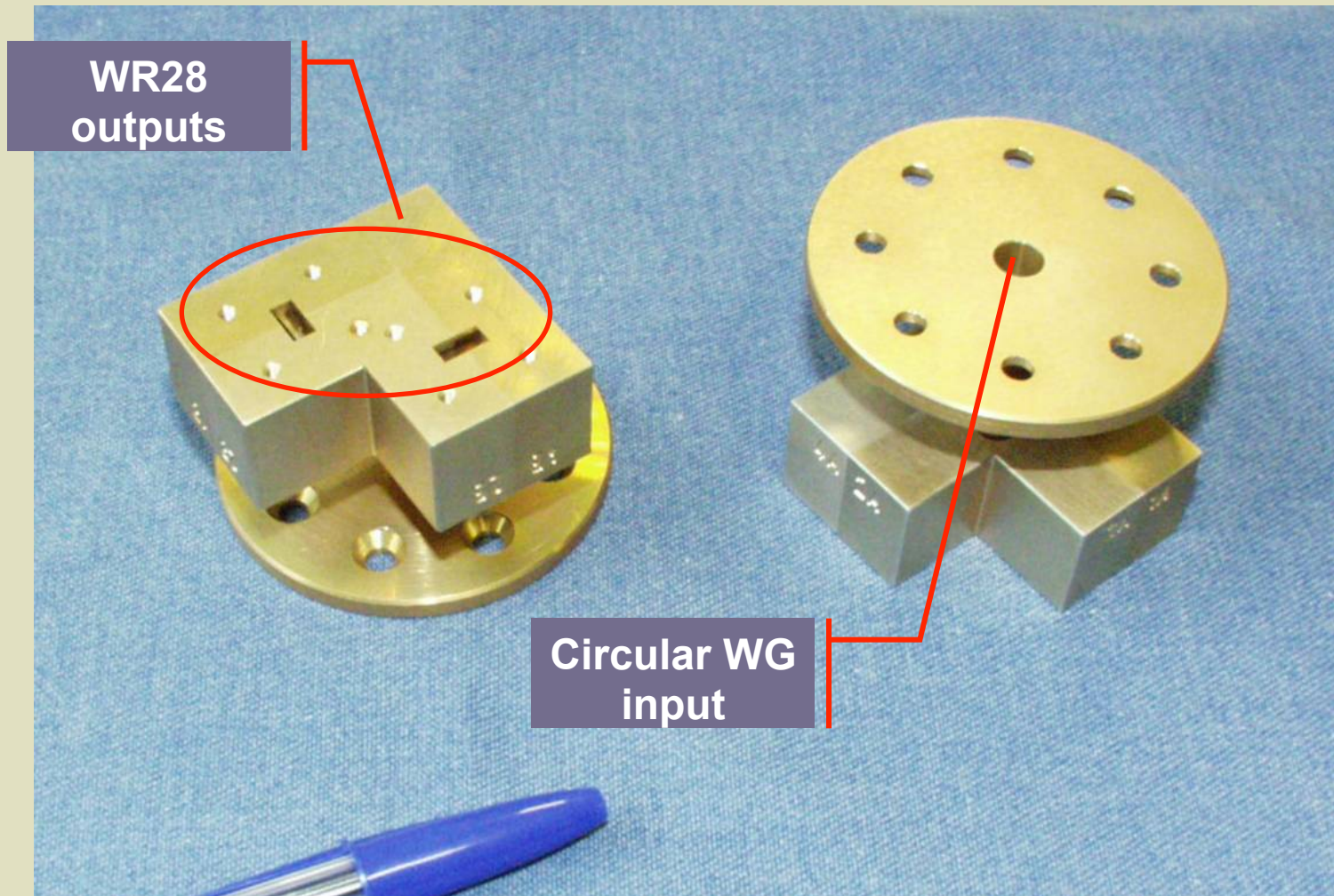
$\Delta\Phi = 90.5^\circ \pm 1.5^\circ$
 $IL < 0.3 \text{ dB}$
 26 to 36 GHz

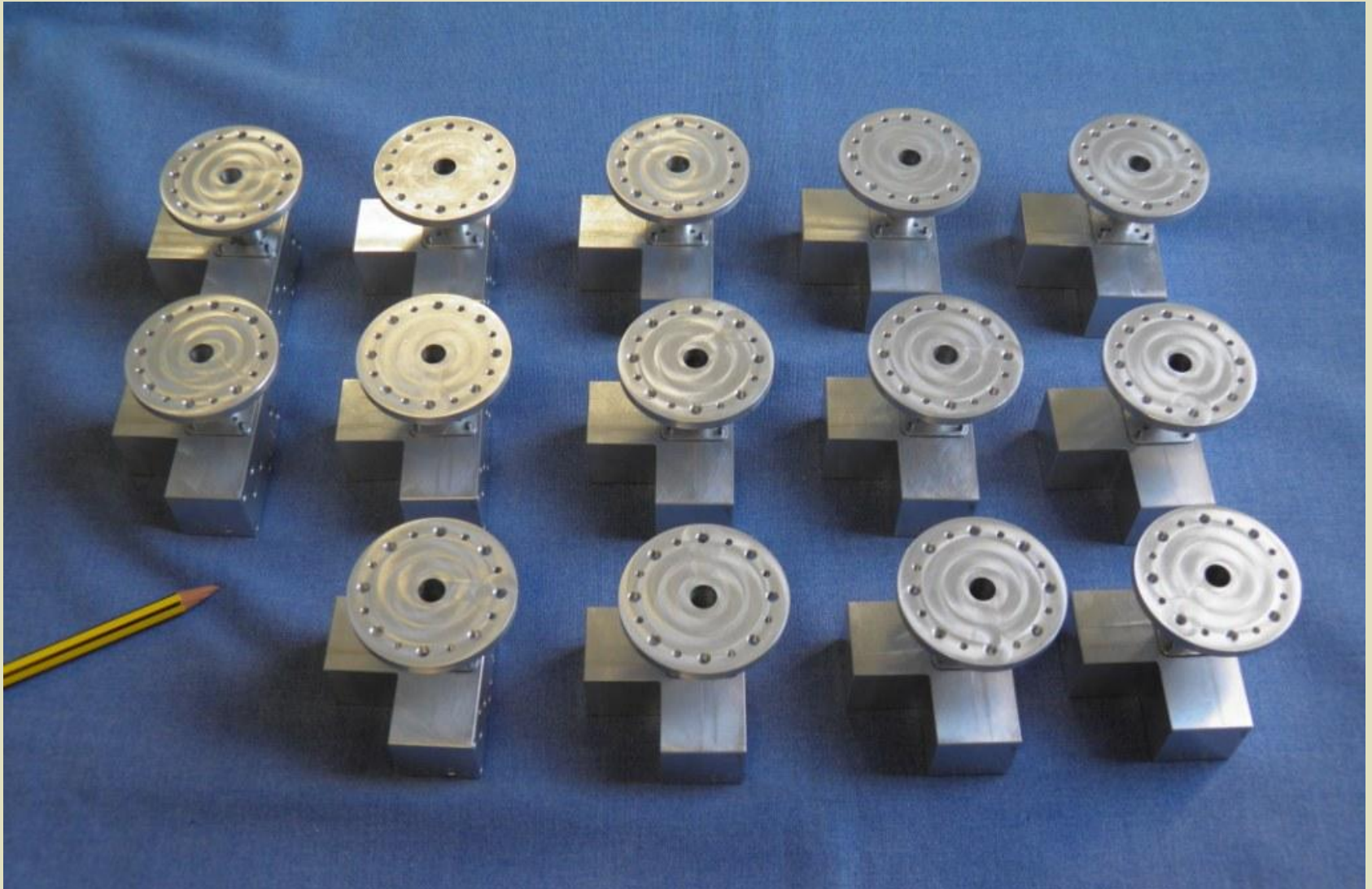


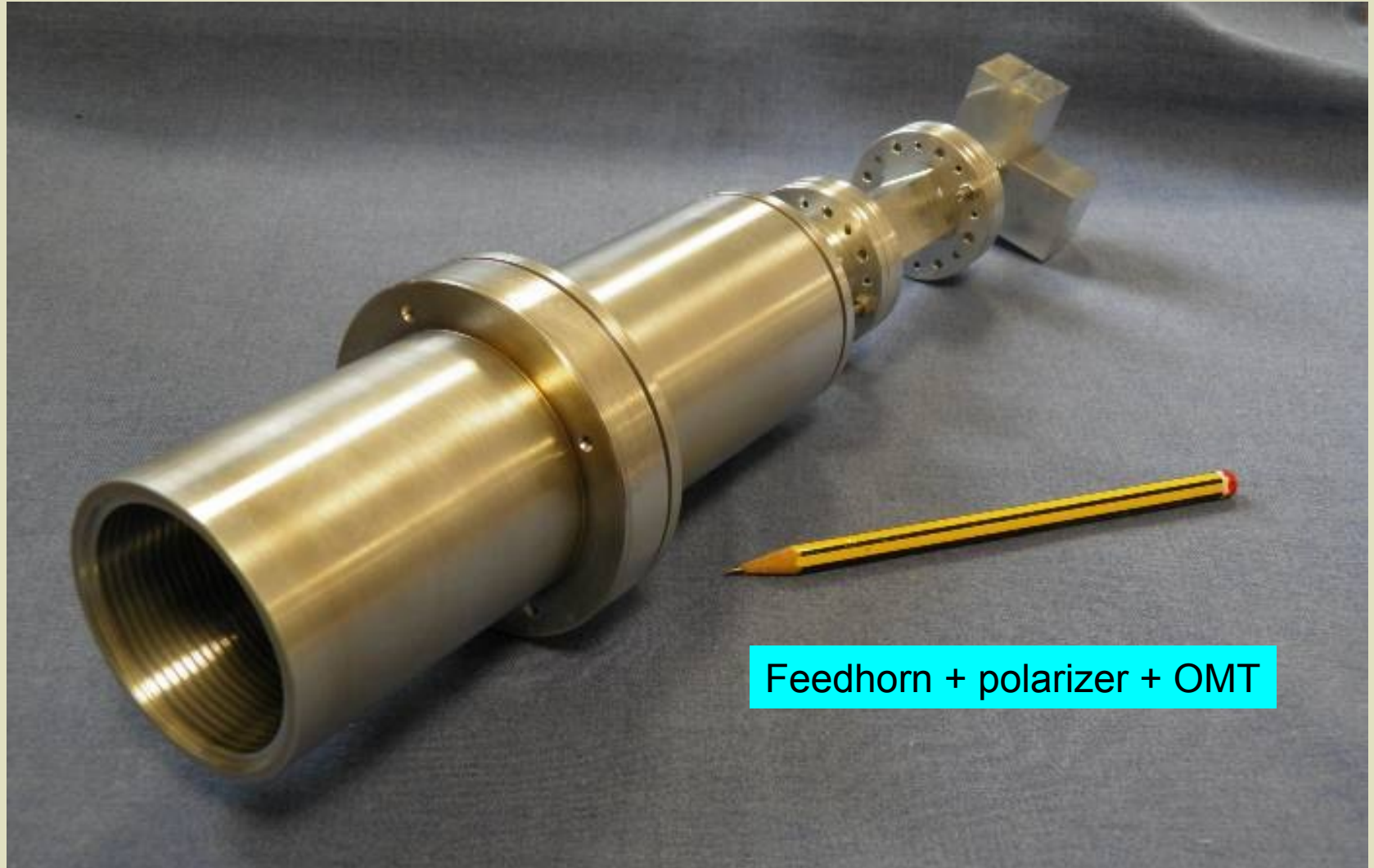
34 polarizers (TGI)



***Orthomode Transducer (OMT) (26-36 GHz)
Same component as for the 1st instrument (MFI)***

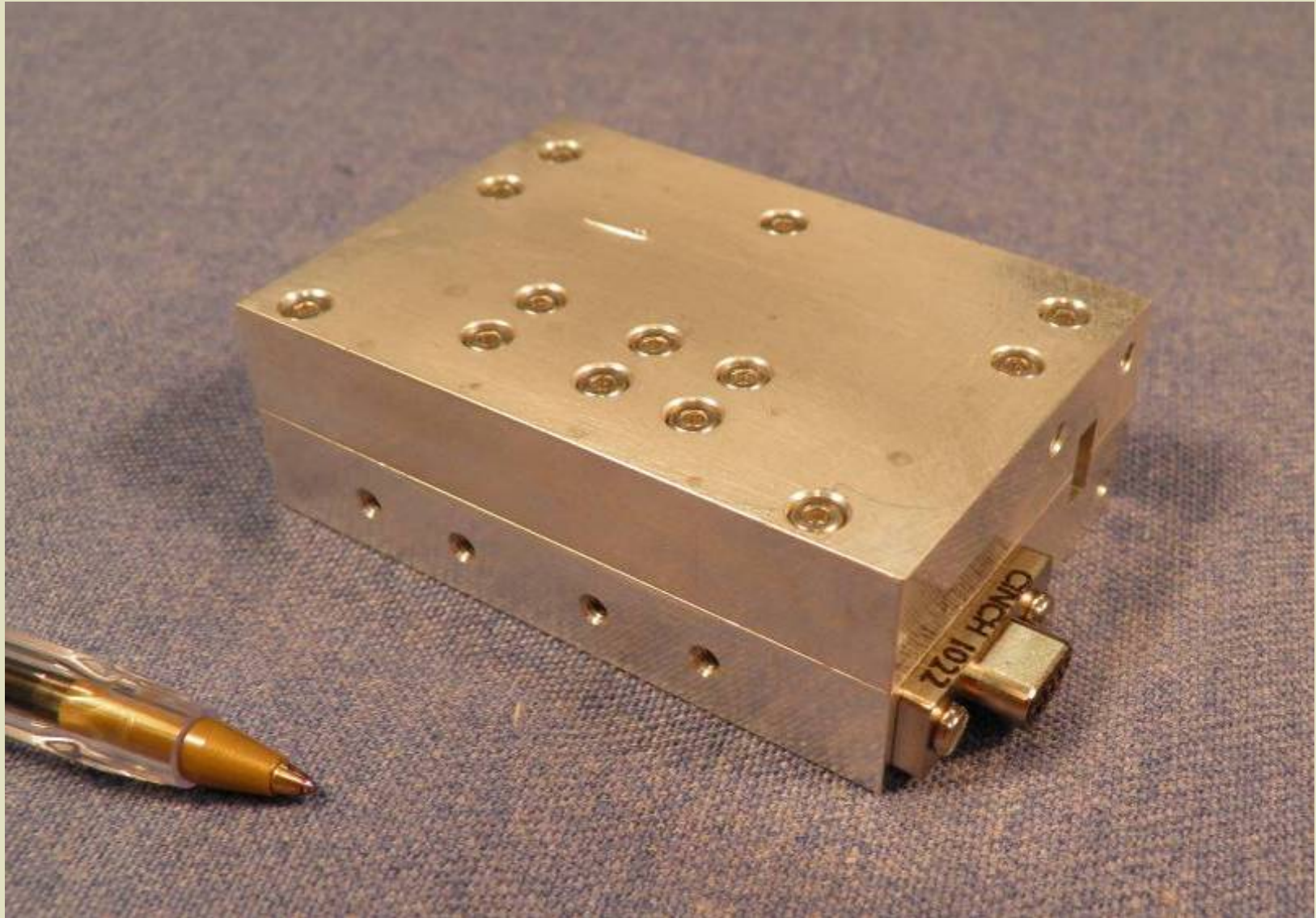


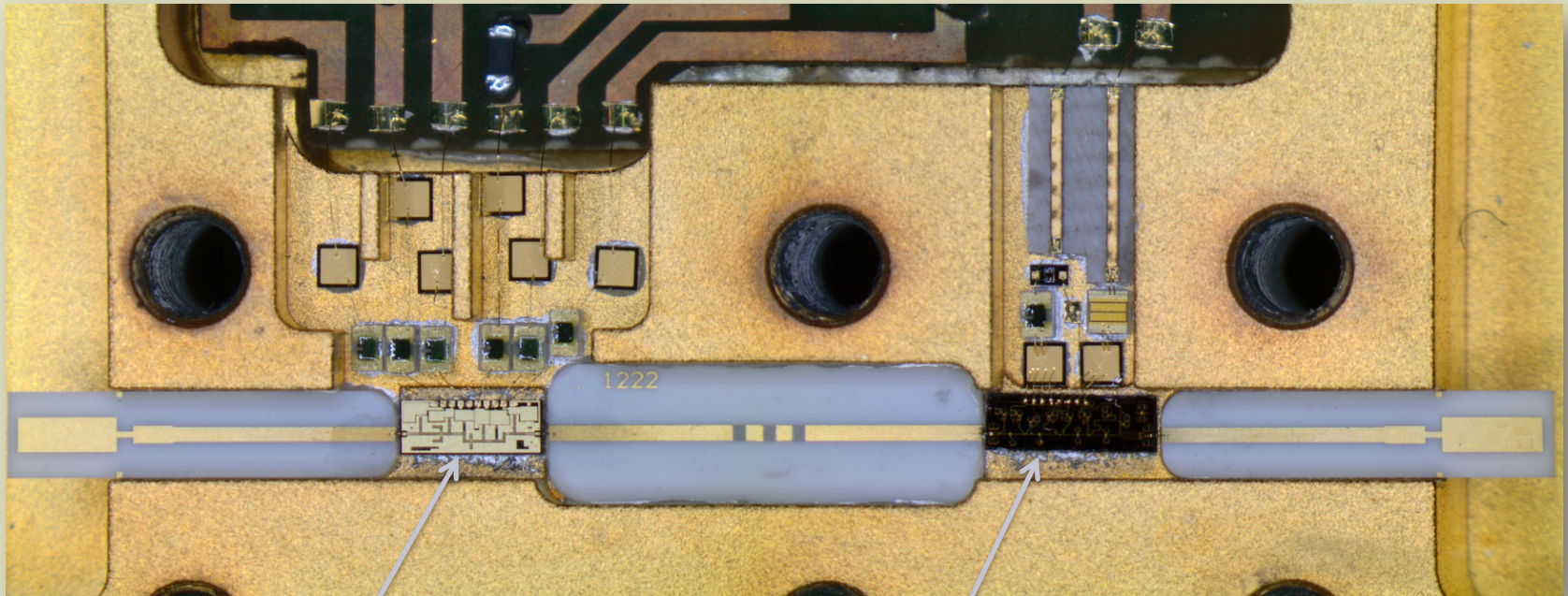




Feedhorn + polarizer + OMT

Cryo-LNA (FEM) 26-36 GHz - Prototype

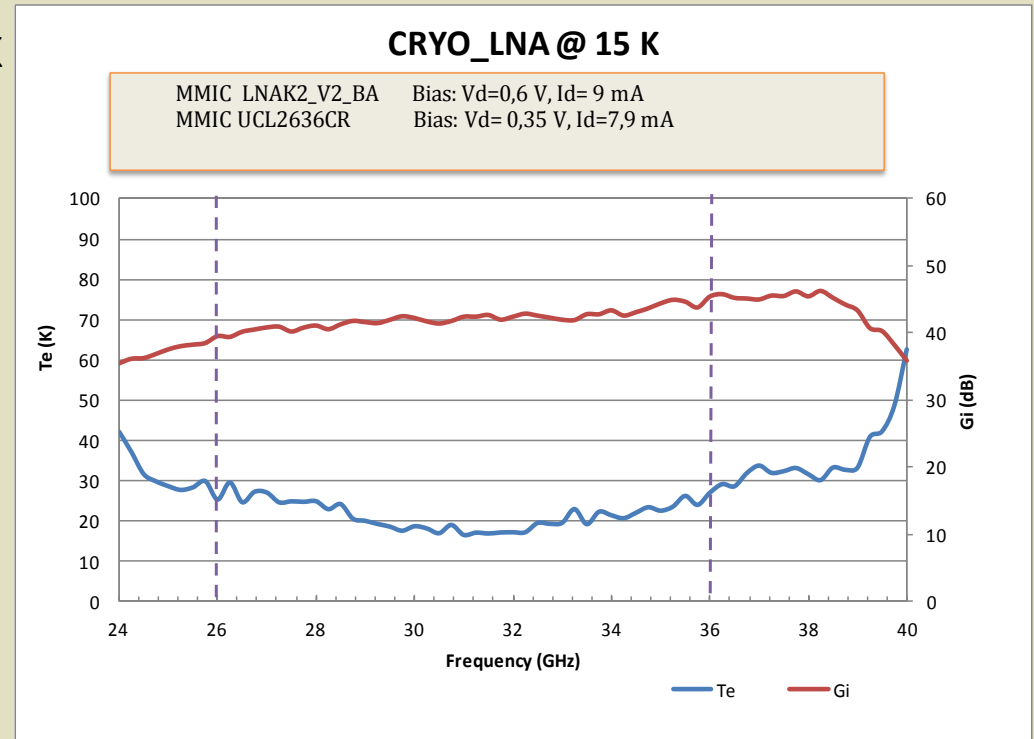




- ✓ ALN002MAKA_AB_S2 (IAF) (C17) + UCL2636CR (OMMIC) (Wafer 6984)
- ✓ 5 dB Attenuator between chips

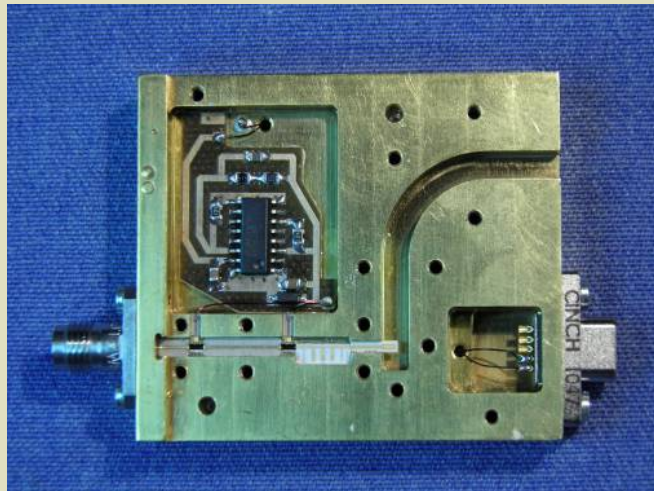
DC consumption (1 cryo_LNA) @ 15K

	Vd	Id	Power
1 st MMIC	0.6 Volt.	9 mA	5.4 mW
2 nd MMIC	0.35 Volt.	8 mA	2.8 mW
Total			8.2 mW

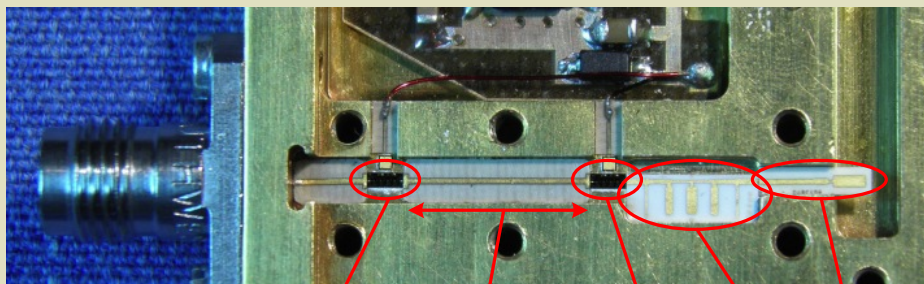
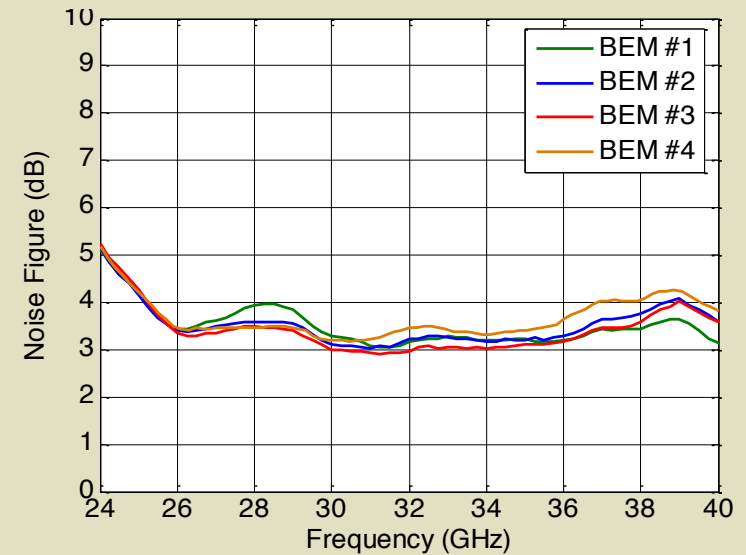
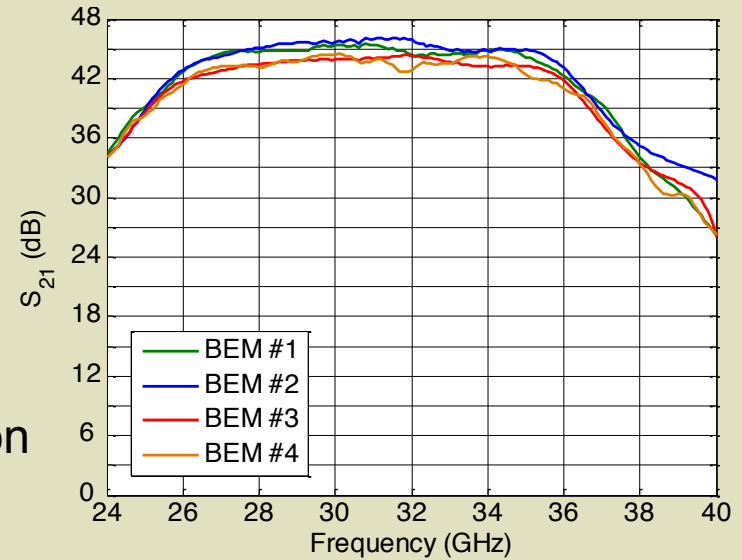


Freq	Te (avg), K	Te (min), K	Gi (avg), dB
26-36 GHz	21,6	16,6	42,1

- Gain: $G \sim 44$ dB
- Noise Figure < 4 dB
- 26-36 GHz



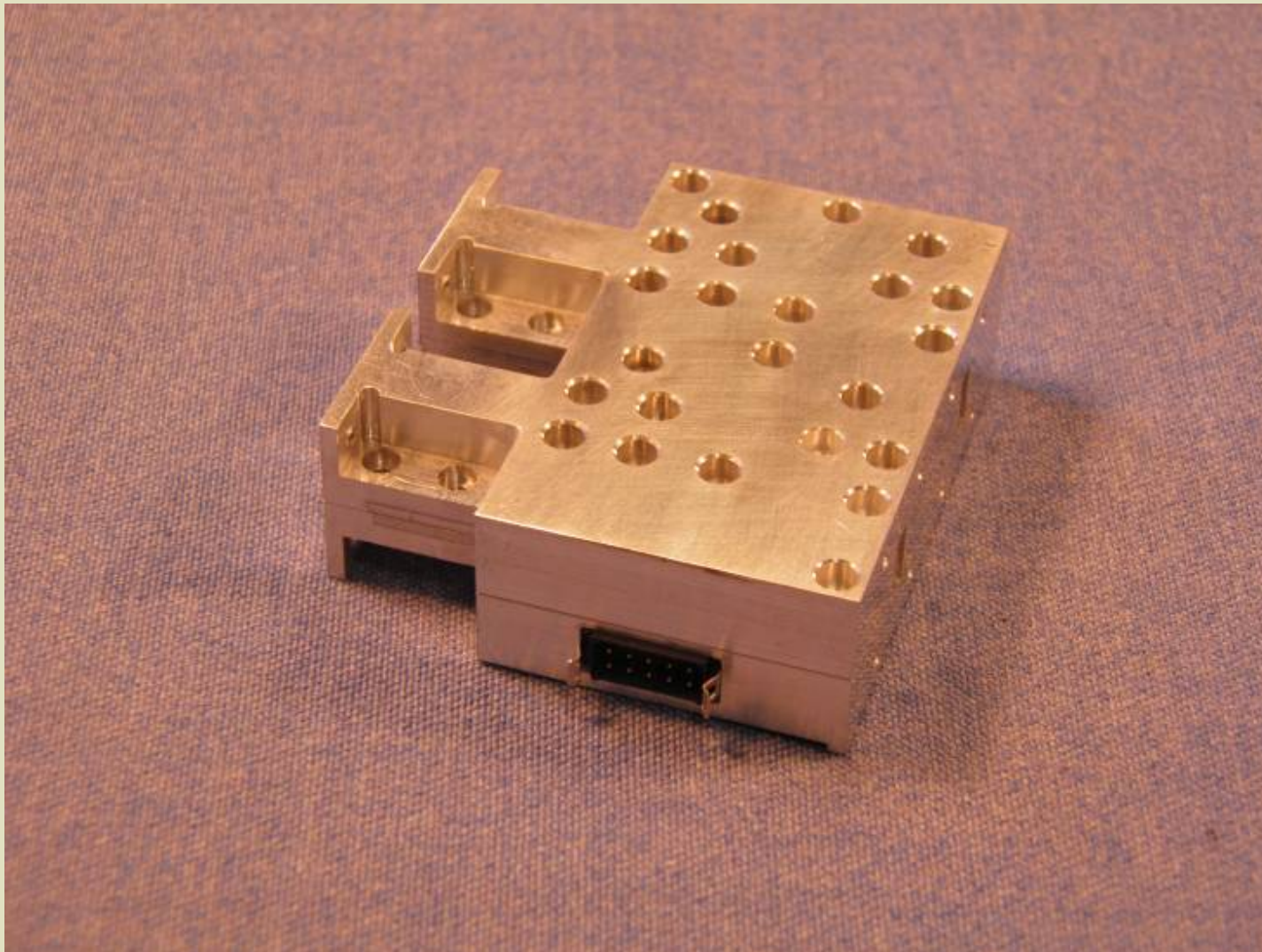
4 units
comparison



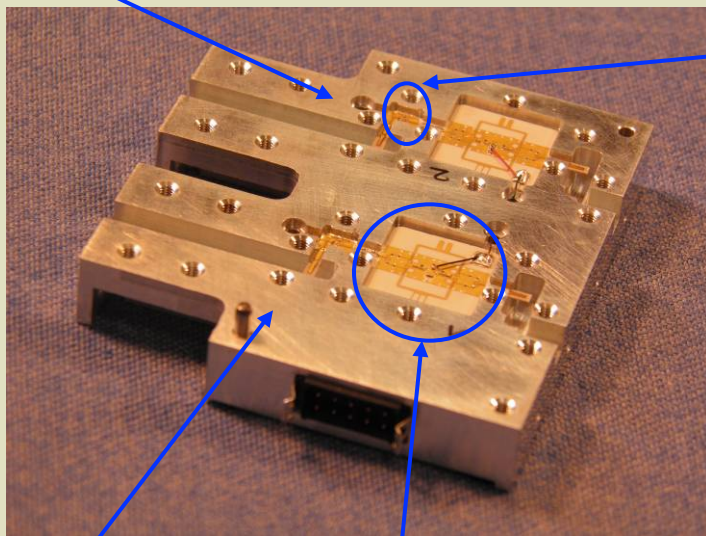
LNA #1 Space for Attenuator LNA #2 BPF Transition



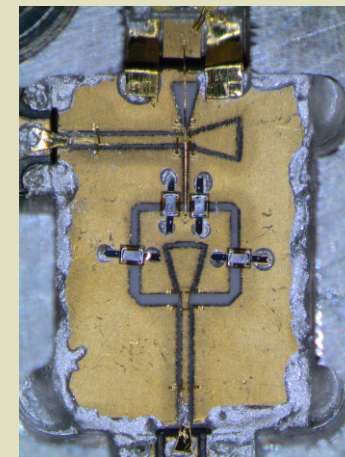
RF Gain (BEM): 32 of 62
(30 in this picture)



Branch #2

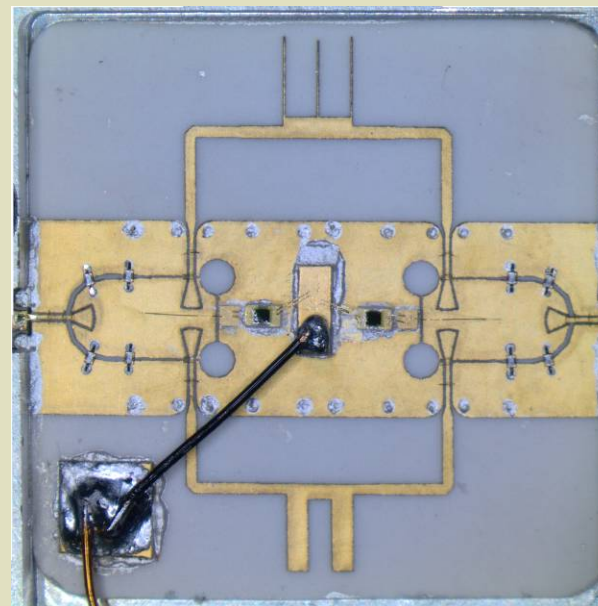


180° Phase
Switch

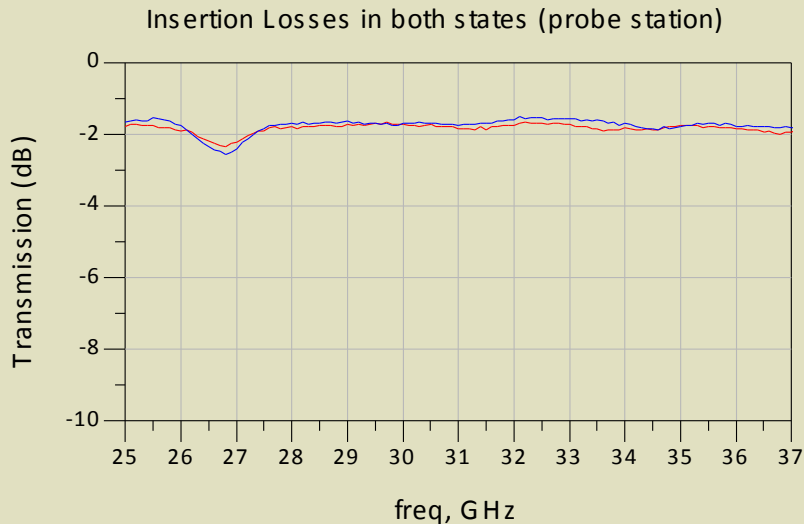
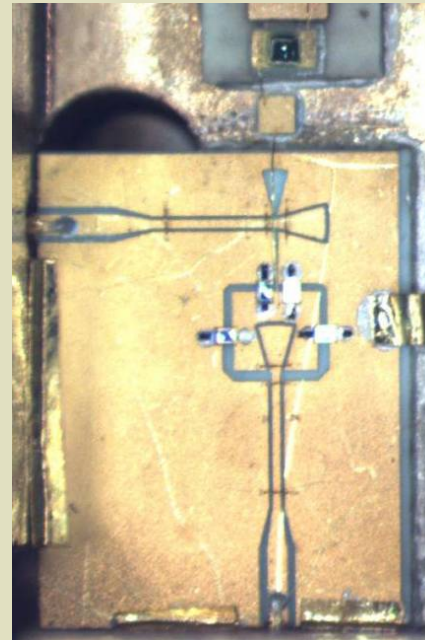


Branch #1

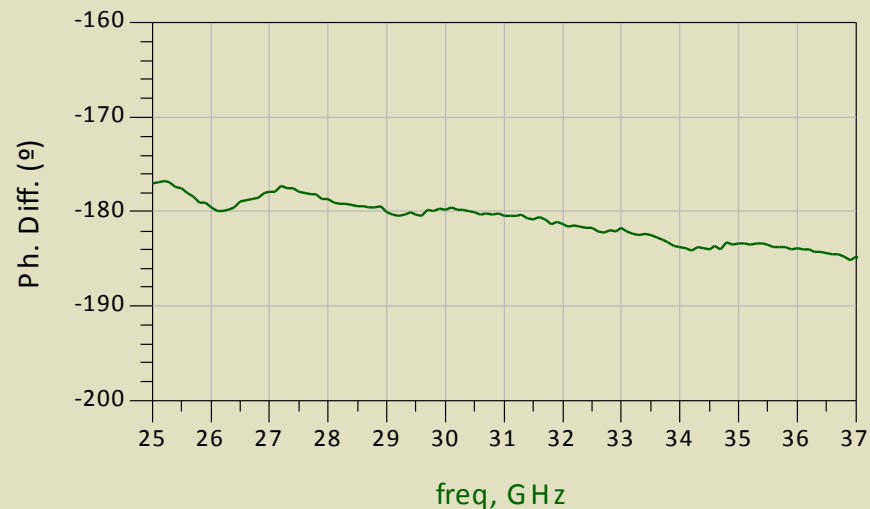
90° Phase
Switch



Coplanar-slot switch with PIN diodes



Phase Diff. (probe station) - PIN Diode HPND4005



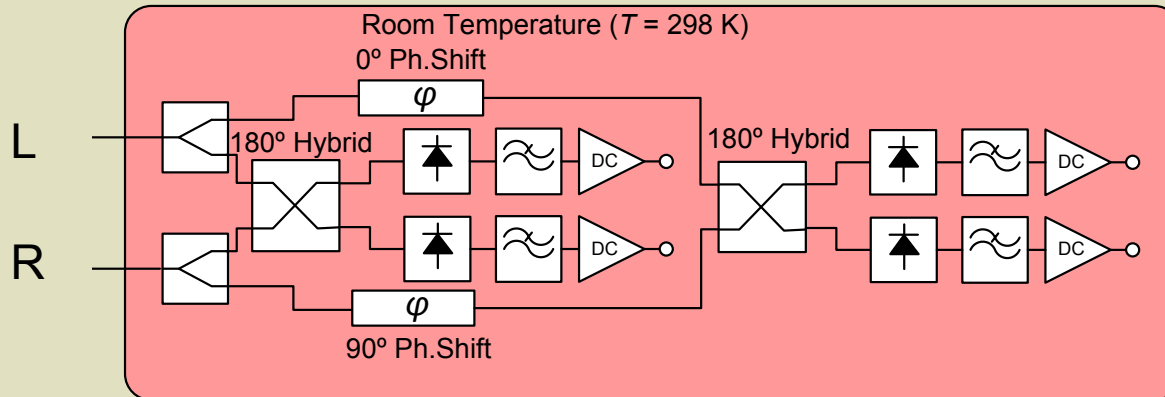
Coplanar probe station tests

$$I_T = 40 \text{ mA}$$

$$\Phi = 181^\circ \text{ (mean value in 26-36 GHz)}$$

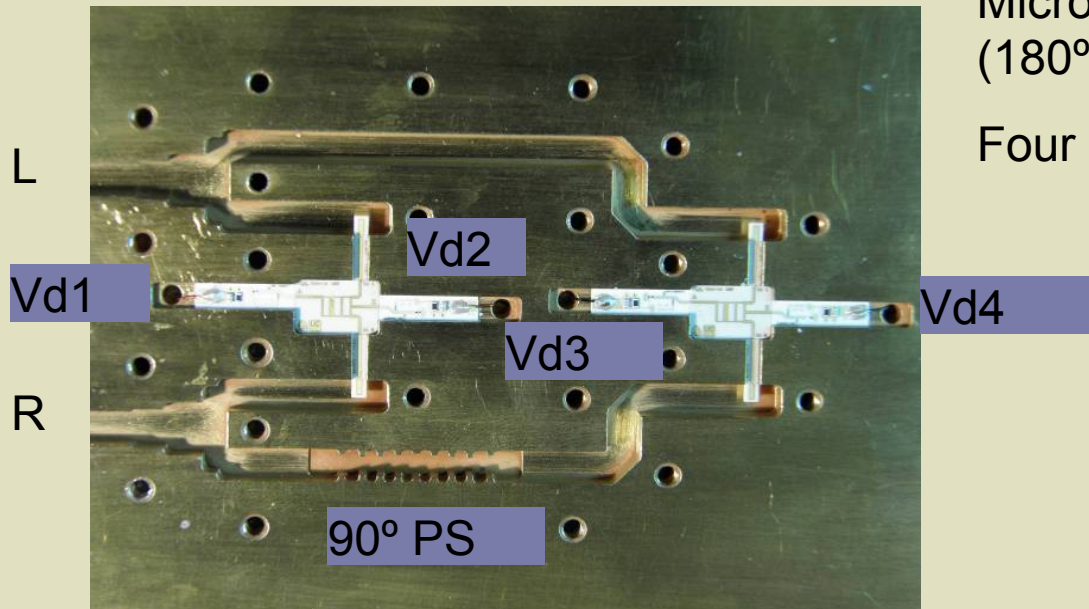
$$\Delta\Phi = \pm 2.5^\circ$$

$$\text{IL imbalance (26-36 GHz)} \leq 0.2 \text{ dB}$$

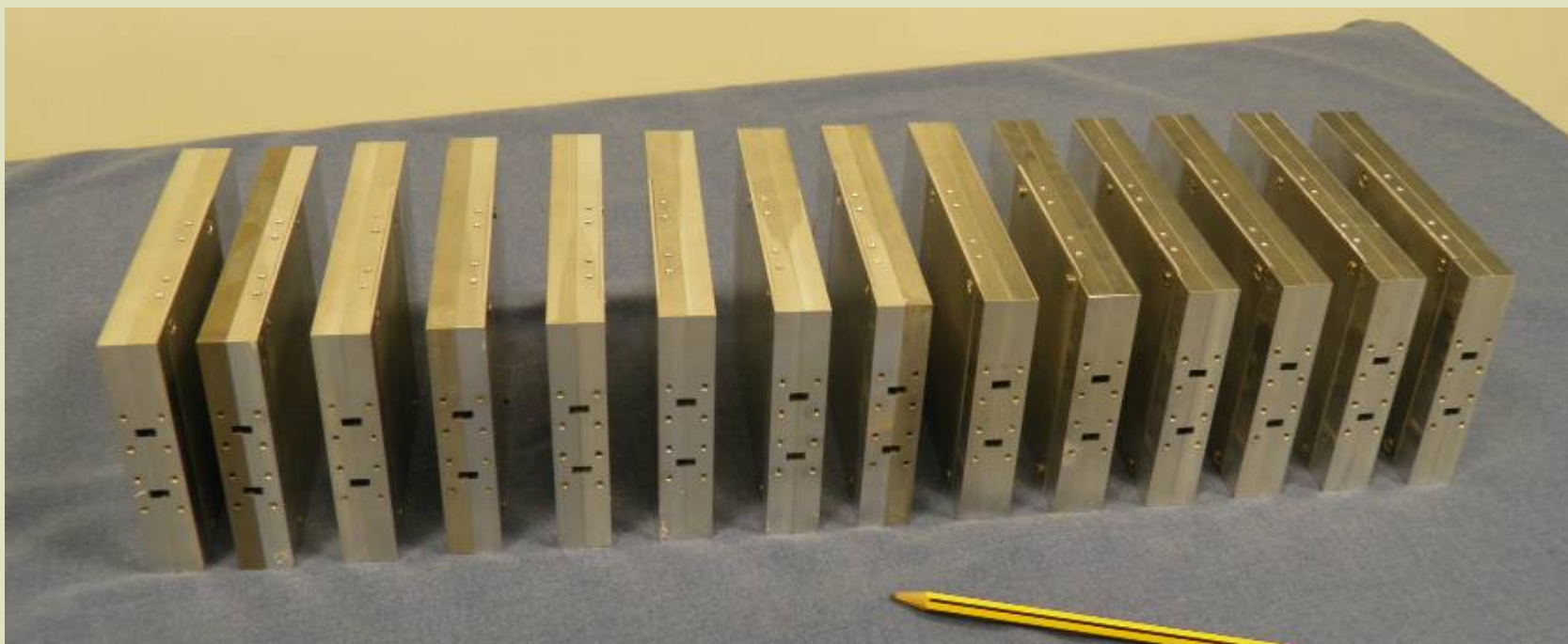


Microwave correlation (26-36 GHz)
(180° hybrids)

Four detected outputs

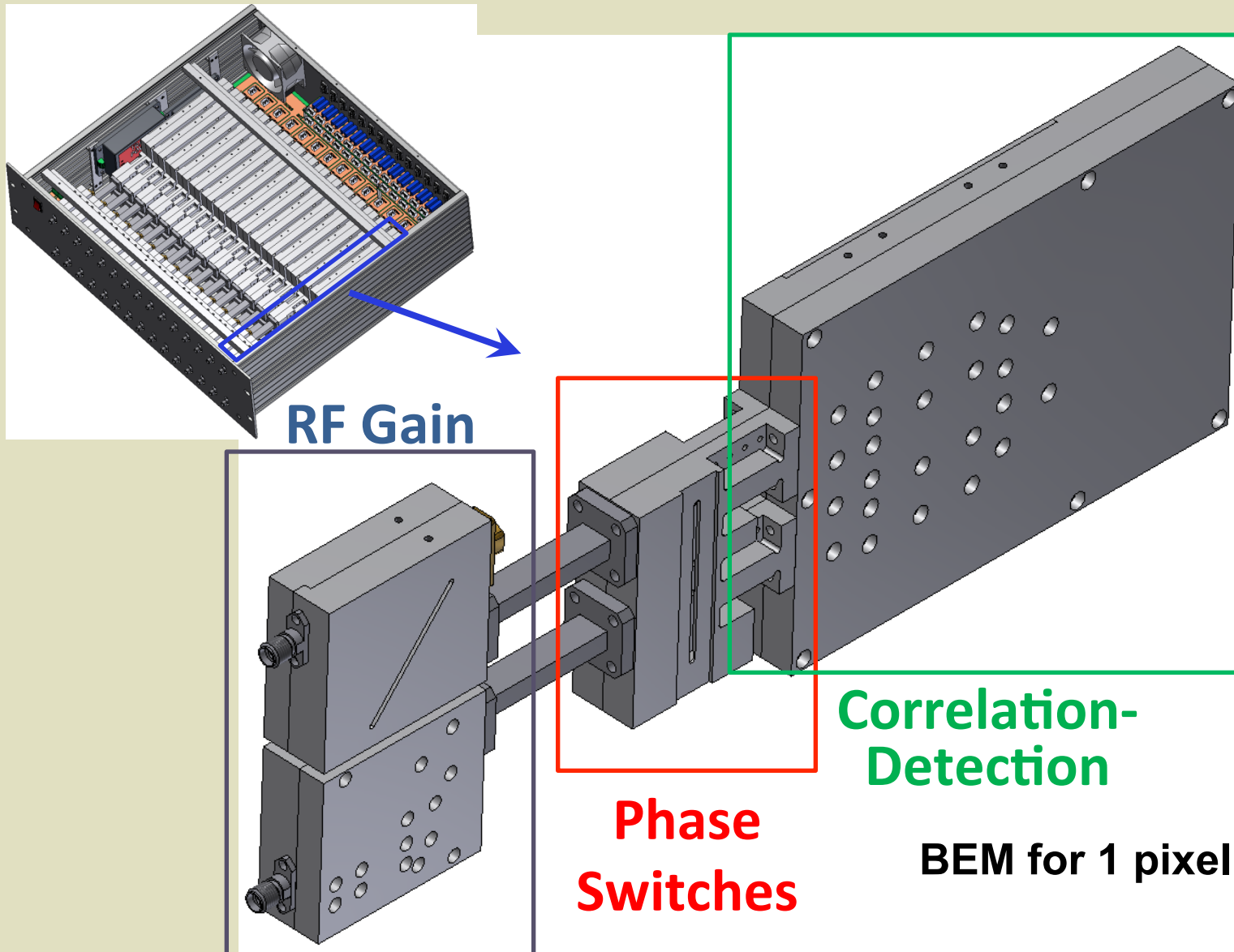


3 dB/180° broadband hybrid

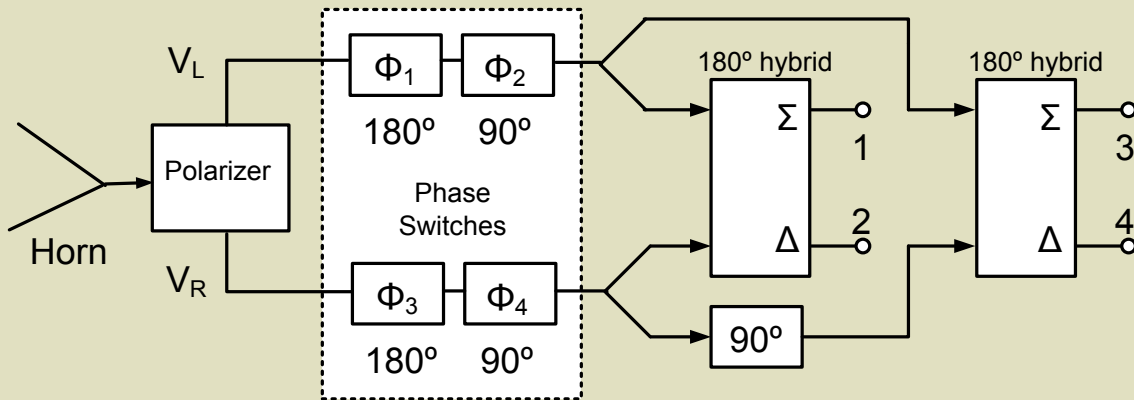


Correlation-Detection (BEM): 20 of 31
(14 in this picture)

BEM rack assembly: 1 unit of 16



Stokes parameters from detected voltages



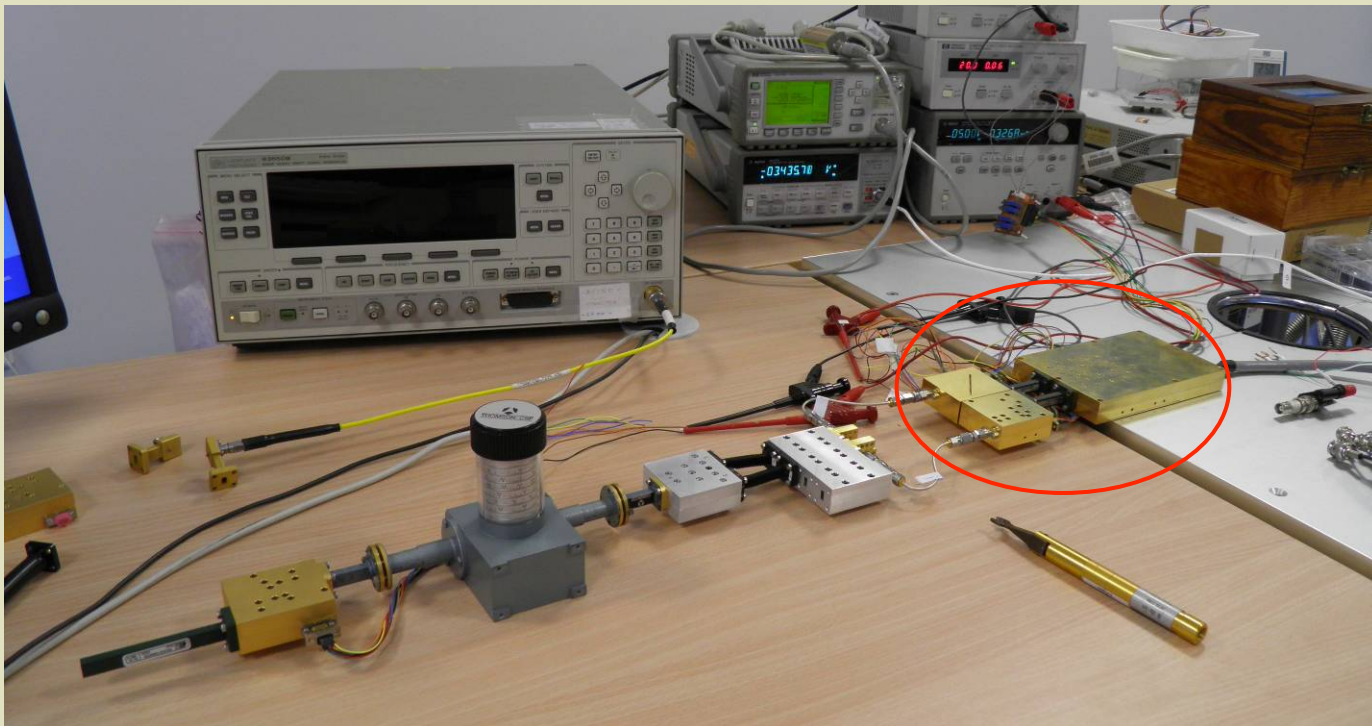
Stokes parameters:

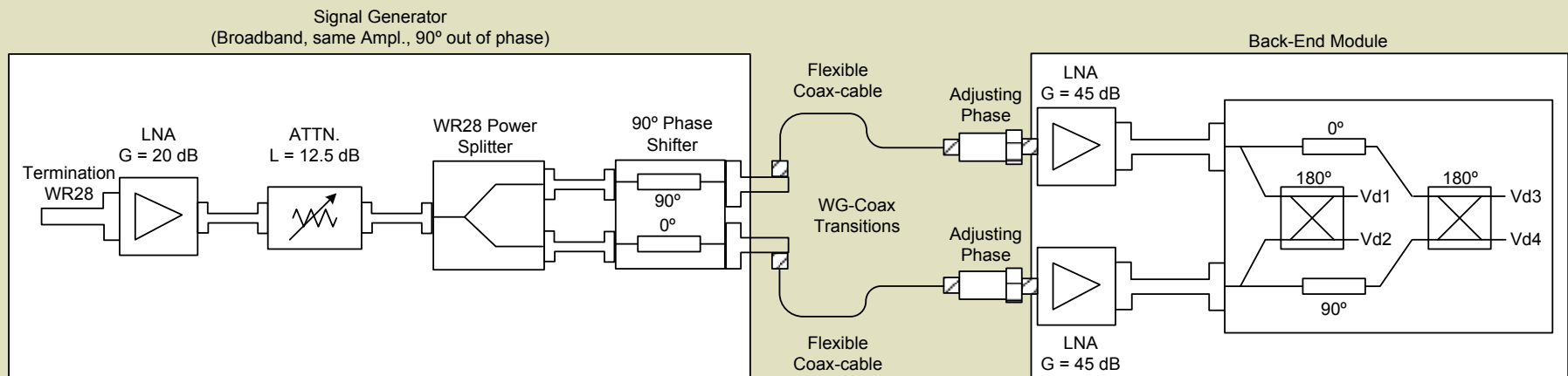
I = Intensity (power)

Q and U = linear polarisation

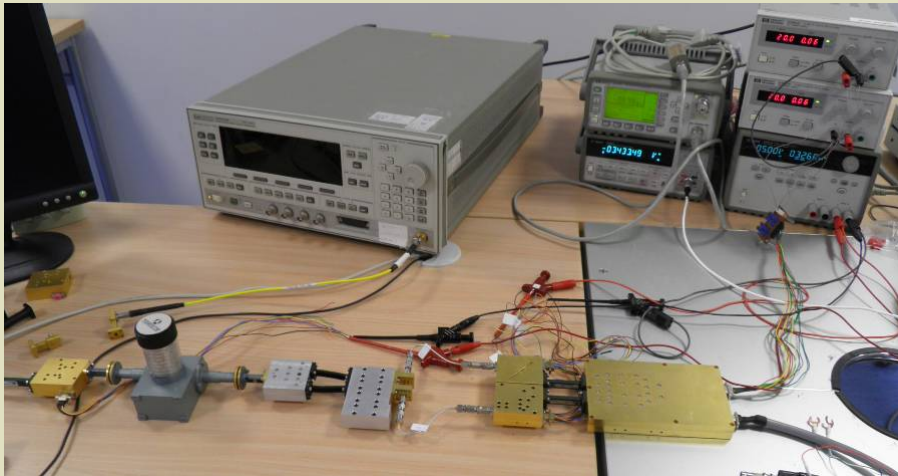
Φ	I	Q	U
0°	$V_{d1} + V_{d2} = V_{d3} + V_{d4}$	$V_{d1} - V_{d2}$	$V_{d3} - V_{d4}$
90°	$V_{d1} + V_{d2} = V_{d3} + V_{d4}$	$V_{d3} - V_{d4}$	$V_{d2} - V_{d1}$
180°	$V_{d1} + V_{d2} = V_{d3} + V_{d4}$	$V_{d2} - V_{d1}$	$V_{d4} - V_{d3}$
270°	$V_{d1} + V_{d2} = V_{d3} + V_{d4}$	$V_{d4} - V_{d3}$	$V_{d1} - V_{d2}$

- Linearly polarized wave at feed-horn input \Rightarrow two signals with the same amplitude and 90° out of phase at the OMT outputs
- In the laboratory: two **broadband** signals generation with the same amplitude and 90° out of phase to be introduced to the BEM.





- Input: **Broadband noise**
- Two signals at BEM input: same amplitude, phase shift 90°: $-jA$ and A
- “Adjusting Phase” to minimize difference output (Vd4)



Broadband noise (input)

Detected voltages
(differential outputs of DC amplifiers):

Test result	Theory
Vd1 = 1.75 V	(A ² /2)
Vd2 = 1.87 V	(A ² /2)
Vd3 = 3.07 V	(A ²)
Vd4 = 0.92 V	(0)

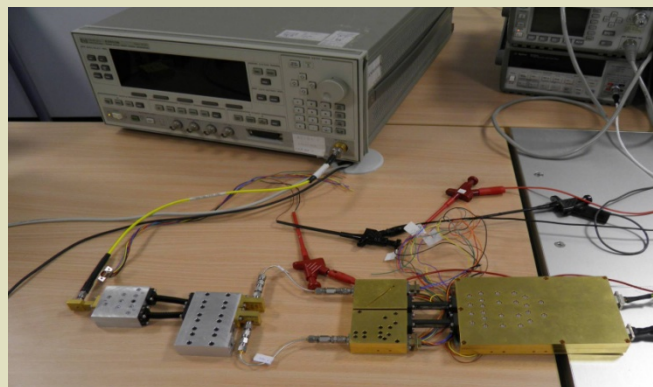
Stokes parameters (without voltage normalization):

$I = Vd1 + Vd2 = 3.62 \text{ V}$ (alt. $Vd3 + Vd4 = 3.99 \text{ V}$)	$I = A^2$
$Q = Vd1 - Vd2 = -0.12 \text{ V}$	$Q = 0$
$U = Vd3 - Vd4 = 2.15 \text{ V}$	$U = A^2$

Isolation parameters (Figures of merit):

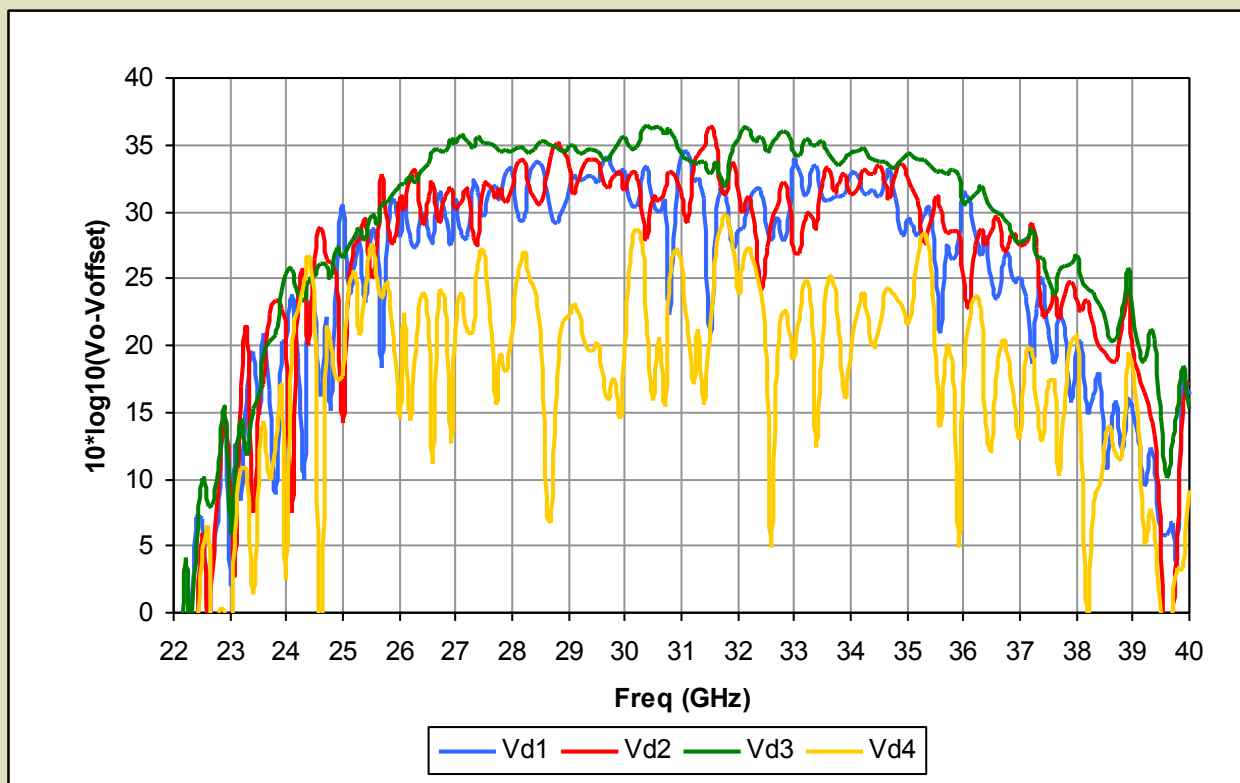
$Isol1 = 10 \log I/Q = 14.8 \text{ dB}$	(leakage I to Q)
$Isol2 = 10 \log U/Q = 12.5 \text{ dB}$	(leakage U to Q)

Input: Pgen = -60 dBm
22 to 40 GHz



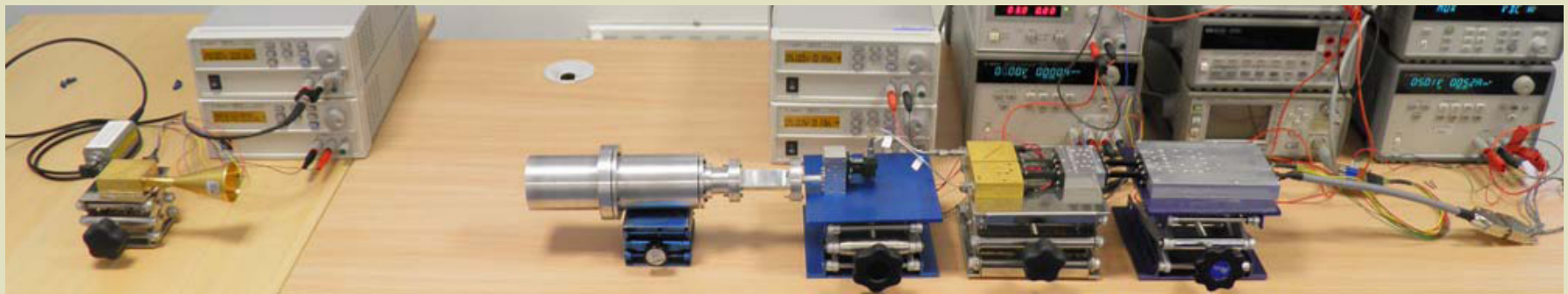
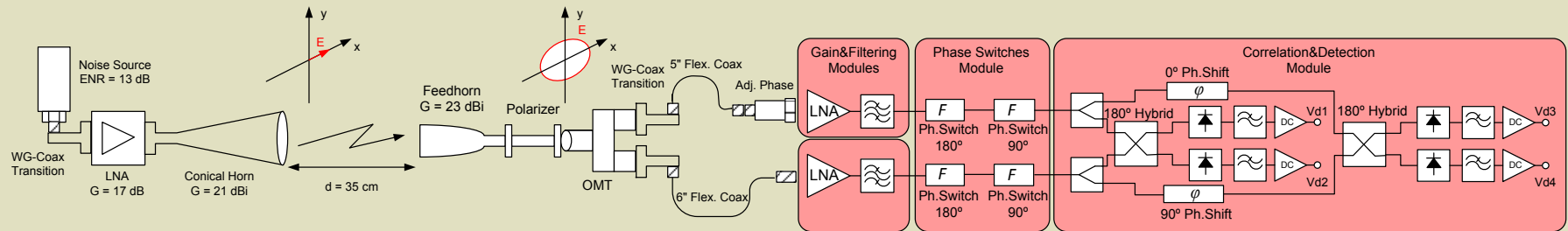
Theoretical
detected outputs

- $A^2/2$
- $A^2/2$
- A^2
- 0



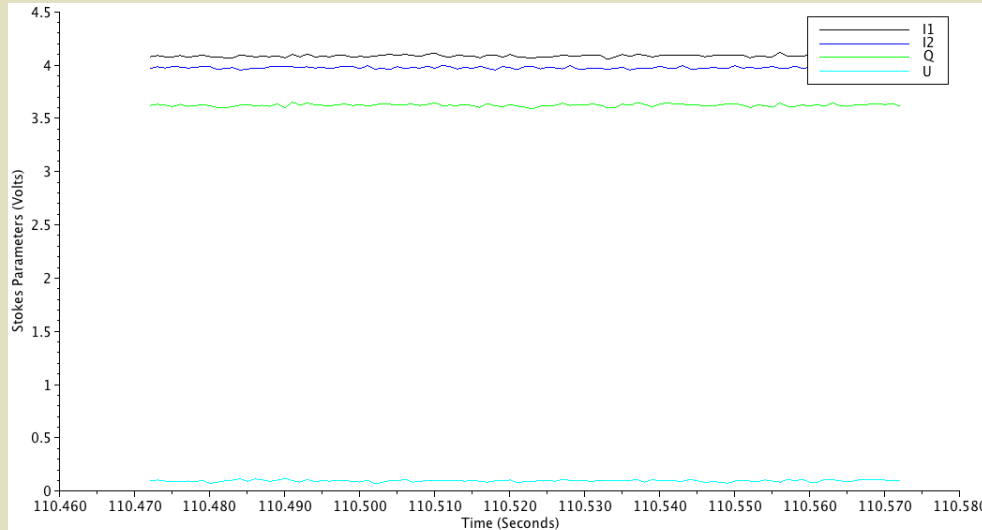
Input: Broadband linearly polarized signal (from a Noise source)

Radiometer outputs (1, 2, 3 and 4): detected signals proportional to power





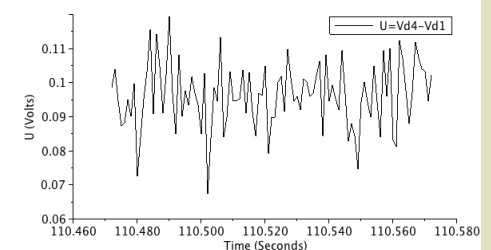
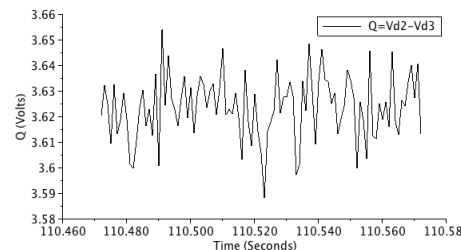
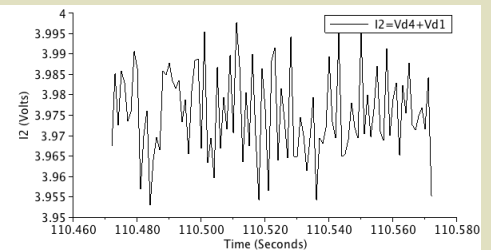
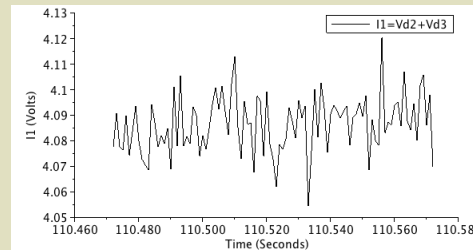
Measurement at 1 Hz sampling frequency



Efficiency = $Q/I = 89.8\%$
Isolation = $U/Q = -15.6 \text{ dB}$

Stokes parameters

$$\begin{aligned}
 V2+V3=4.09 &\Rightarrow I_1 = 1.0 \\
 V4+V1=3.98 &\Rightarrow I_2 = 0.97 \\
 I=(I1+I2)/2 &\Rightarrow I = 0.98 \\
 V2-V3=3.62 &\Rightarrow Q = 0.88 \\
 V4-V1=0.1 &\Rightarrow U = 0.024
 \end{aligned}$$



- **Phase switching receiver operation demonstrated experimentally (and confirmed by simulations).**
- **Good isolation of Stokes parameters requires adjusting phase and amplitude (between the two branches).**
- **Stokes parameters can be obtained from outputs.**
- **Receiver FEM and BEM subsystems under manufacturing.**

Acknowledgment

QUIJOTE experiment is funded by the Spanish Ministry of Science and Innovation.

Reference: AYA2010-21766-C03



For further information visit:
<http://www.iac.es/project/cmb/quijote/index.php>